



# Illinois Environmental Protection Agency

Bureau of Land • 1021 N. Grand Avenue E. • P.O. Box 19276 • Springfield • Illinois • 62794-9276

## HIGHWAY AUTHORITY AGREEMENT

This Agreement is entered into this \_\_\_\_\_ day of \_\_\_\_\_, 20\_\_\_\_ pursuant to 35 Ill. Adm. Code 742.1020 by and between the (1) \_\_\_\_\_ Flip 25, LLC \_\_\_\_\_ (“Property Owner”) [*or, in the case of a petroleum leaking underground storage tank (UST), the owner/operator of the tank (“Owner/Operator”)*] and (2) \_\_\_\_\_ City of Aurora \_\_\_\_\_ [*Name of Entity in Control of the Right-of-Way*] (“Highway Authority”), collectively known as the “Parties.”

[*Use this paragraph for sites with petroleum leaking underground storage tank(s)*]  
WHEREAS, \_\_\_\_\_ Flip 25, LLC \_\_\_\_\_ is the owner or operator of one or more leaking underground storage tanks presently or formerly located at \_\_\_\_\_ 1125 Aurora Avenue, Aurora \_\_\_\_\_ (“the Site”);

[*Use this paragraph for sites that do not have petroleum leaking USTs*]  
WHEREAS, \_\_\_\_\_ is the owner of the property located at \_\_\_\_\_ (“the Site”);

**WHEREAS**, as a result of one or more releases of contaminants \_\_\_\_\_ at the above referenced Site (“the Release(s)”), soil and/or groundwater contamination at the Site exceeds the Tier 1 residential remediation objectives of 35 Ill. Adm. Code 742;

**WHEREAS**, the soil and/or groundwater contamination exceeding Tier 1 residential remediation objectives extends or may extend into the Highway Authority’s right-of-way;

**WHEREAS**, the Owner/Operator or Property Owner is conducting corrective action in response to the Release(s);

**WHEREAS**, the Parties desire to prevent groundwater beneath the Highway Authority’s right-of-way that exceeds Tier 1 remediation objectives from use as a supply of potable or domestic water and to limit access to soil within the right-of-way that exceeds Tier 1 residential remediation objectives so that human health and the environment are protected during and after any access;

**NOW, THEREFORE**, the Parties agree as follows:

1. The recitals set forth above are incorporated by reference as if fully set forth herein.
2. [*Use this paragraph if IEMA has issued an incident number*] The Illinois Emergency Management Agency has assigned incident number(s) \_\_\_\_\_ 20190483 \_\_\_\_\_ to the Release(s).
3. Attached as Exhibit A is a scaled map(s) prepared by the \_\_\_\_\_ Property Owner \_\_\_\_\_ that shows the Site and surrounding area and delineates the current and estimated future extent of soil and groundwater contamination above the applicable Tier 1 residential remediation objectives as a result of the Release(s).  
[*Use the following sentence if either soil or groundwater is not contaminated above applicable Tier 1 residential remediation objectives:* \_\_\_\_\_ Soil \_\_\_\_\_ is not contaminated above the applicable Tier 1 residential remediation objectives.]
4. Attached as Exhibit B is a table(s) prepared by the \_\_\_\_\_ Property Owner \_\_\_\_\_ that lists each contaminant of concern that exceeds its Tier 1 residential remediation objective, its Tier 1 residential remediation objective and its concentrations within the zone where Tier 1 residential remediation objectives are exceeded. The locations of the concentrations listed in Exhibit B are identified on the map(s) in Exhibit A.

5. Attached as Exhibit C is a scaled map prepared by the Owner/Operator showing the area of the Highway Authority's right-of-way that is governed by this agreement ("Right-of-Way"). Because Exhibit C is not a surveyed plat, the Right-of-Way boundary may be an approximation of the actual Right-of-Way lines.
6. *[Use this paragraph if samples have not been collected within the Right-of-Way, sampling within the Right-of-Way is not practical, and contamination does not extend beyond the Right-of-Way.]* Because the collection of samples within the Right-of-Way is not practical, the Parties stipulate that, based on modeling, soil and groundwater contamination exceeding Tier 1 residential remediation objectives does not and will not extend beyond the boundaries of the Right-of-Way.
7. The Highway Authority stipulates it has jurisdiction over the Right-of-Way that gives it sole control over the use of the groundwater and access to the soil located within or beneath the Right-of-Way.
8. The Highway Authority agrees to prohibit within the Right-of-Way all potable and domestic uses of groundwater exceeding Tier 1 residential remediation objectives.
9. The Highway Authority further agrees to limit access by itself and others to soil within the Right-of-Way exceeding Tier 1 residential remediation objectives. Access shall be allowed only if human health (including worker safety) and the environment are protected during and after any access. The Highway Authority may construct, reconstruct, improve, repair, maintain and operate a highway upon the Right-of-Way, or allow others to do the same by permit. In addition, the Highway Authority and others using or working in the Right-of-Way under permit have the right to remove soil or groundwater from the Right-of-Way and dispose of the same in accordance with applicable environmental laws and regulations. The Highway Authority agrees to issue all permits for work in the Right-of-Way, and make all existing permits for work in the Right-of-Way, subject to the following or a substantially similar condition:

As a condition of this permit the permittee shall request the office issuing this permit to identify sites in the Right-of-Way where a Highway Authority Agreement governs access to soil that exceeds the Tier 1 residential remediation objectives of 35 Ill. Adm. Code 742. The permittee shall take all measures necessary to protect human health (including worker safety) and the environment during and after any access to such soil.

10. This agreement shall be referenced in the Agency's no further remediation determination issued for the Release(s).
11. The Agency shall be notified of any transfer of jurisdiction over the Right-of-Way at least 30 days prior to the date the transfer takes effect. This agreement shall be null and void upon the transfer unless the transferee agrees to be bound by this agreement as if the transferee were an original party to this agreement. The transferee's agreement to be bound by the terms of this agreement shall be memorialized at the time of transfer in a writing ("Rider") that references this Highway Authority Agreement and is signed by the Highway Authority, or subsequent transferor, and the transferee.
12. This agreement shall become effective on the date the Agency issues a no further remediation determination for the Release(s). It shall remain effective until the Right-of-Way is demonstrated to be suitable for unrestricted use and the Agency issues a new no further remediation determination to reflect there is no longer a need for this agreement, or until the agreement is otherwise terminated or voided.
13. In addition to any other remedies that may be available, the Agency may bring suit to enforce the terms of this agreement or may, in its sole discretion, declare this agreement null and void if any of the Parties or any transferee violates any term of this agreement. The Parties or transferee shall be notified in writing of any such declaration.
14. This agreement shall be null and void if a court of competent jurisdiction strikes down any part or provision of the agreement.
15. This agreement supersedes any prior written or oral agreements or understandings between the Parties on the subject matter addressed herein. It may be altered, modified or amended only upon the written consent and agreement of the Parties.
16. Any notices or other correspondence regarding this agreement shall be sent to the Parties at following addresses:

Manager, Division of Remediation Management  
Bureau of Land  
Illinois Environmental Protection Agency  
P.O. Box 19276  
Springfield, IL 62974-9276

\_\_\_\_\_  
(Contact at Highway Authority)

Address \_\_\_\_\_  
City \_\_\_\_\_  
State \_\_\_\_\_  
Zip Code \_\_\_\_\_

Property Owner or Owner/Operator

Name Amaan Fazal

Address 1 S 376 Summit Ave

City Oakbrook Terrace

State IL

Zip Code 60181

IN WITNESS WHEREOF, the Parties have caused this agreement to be signed by their duly authorized representatives.

[NAME OF LOCAL GOVERNMENT]

Date: \_\_\_\_\_

By: \_\_\_\_\_

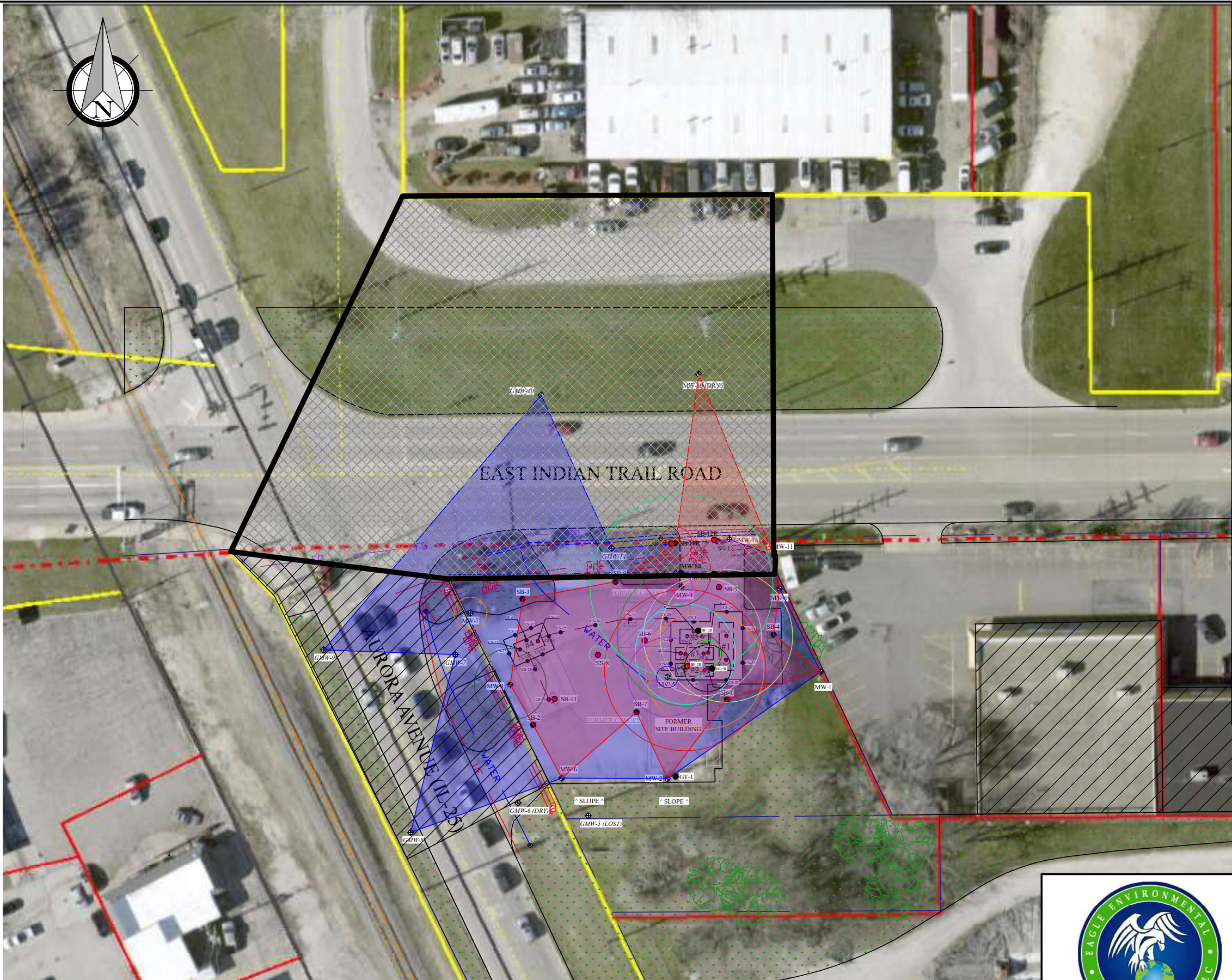
Its: \_\_\_\_\_

Date: \_\_\_\_\_

By: \_\_\_\_\_

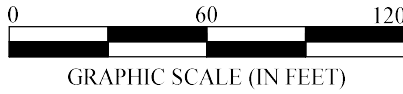
Property Owner or Owner/Operator

Title Manager/Member



**LEGEND**

- CONFIRMATION SAMPLE LOCATION
    - (● = ABOVE TIER 1 SRO'S)
    - (● = ABOVE TIER 1 SOIL SATURATION LIMIT)
    - (● = BELOW TIER 1 SRO'S)
  - SOIL BORING LOCATION
    - (● = ABOVE TIER 1 SRO'S)
    - (● = BELOW TIER 1 SRO'S)
  - MONITORING WELL LOCATION
    - (● = SOIL AND GW BELOW TIER 1 RO'S)
    - (● = SOIL BELOW TIER 1 SRO'S, GW ABOVE TIER 1 GRO'S)
    - (● = SOIL AND GW ABOVE TIER 1 RO'S)
    - (● = GW BELOW TIER 1 RO'S, NO SOIL COLLECTED)
    - (● = GW ABOVE TIER 1 RO'S, NO SOIL COLLECTED)
  - — — — — PROPERTY LINE
  - — — — — FORMER PRODUCT PIPING RUN
  - — — — — OVERHEAD ELECTRIC LINE
  - — — — — UNDERGROUND ELECTRIC LINE
  - — — — — UNDERGROUND FIBER OPTIC LINE
  - — — — — WATER LINE
  - — — — — RAILROAD LINE
  - ⊙ UTILITY POLE
  - ⊙ LIGHT POLE
  - ⊙ FIRE HYDRANT
  - ⊙ STORM SEWER GRATE
- NOTE: MWS LABELED "GMW" WERE INSTALLED BY OTHERS AND CORRESPOND TO LUST INCIDENT #20050170.
- HIGHWAY AUTHORITY AGREEMENT LIMITS (CITY OF AURORA)
  - HIGHWAY AUTHORITY AGREEMENT LIMITS (IDOT)
  - ESTIMATED GROUNDWATER EXTENTS EXCEEDING CLASS I
  - ESTIMATED SOIL EXTENTS EXCEEDING TIER 1
  - MODELED EXTENT



3805 ILLINOIS AVENUE  
ST. CHARLES, ILLINOIS 60174

**PROPOSED HIGHWAY AUTHORITY AGREEMENT LIMITS**

GC REAL ESTATE LLC  
1125 AURORA AVENUE  
AURORA, IL

PREPARED BY: ELMORE	EXHIBIT A	DATE: 03/26/25	PROJECT #: 124121
DRAWN BY: PELLICO	FILE NAME: 124121 - FLIP 25, LLC		

Contaminant	Sample Location	Soil Concentration (mg/kg)	Modeled (or Measured) Concentration (mg/L)	Modeled Distance (ft)
Benzene	CS-1	13.2	0.386	39
	CS-2	7.68	0.225	33
	CS-4	0.0513	0.0015	<Class I
	CS-5	4.63	0.135	28
	CS-6	0.700	0.020	10
	CS-7	24	0.702	45
	CS-8	7.8	0.228	33
	CS-12	0.134	0.0039	<Class I
	CS-19	10.9	0.319	37
	CS-20	0.0703	0.0021	<Class I
	CS-30	0.0645	0.0019	<Class I
	BF-1	0.262	0.0077	3
	BF-2	0.401	0.012	6
	BF-3	0.440	0.013	7
	BF-4	0.609	0.018	10
	BF-5	0.925	0.027	13
	MW-4 (7'-8')	0.360	0.011	6
	MW-5 (7'-9')	0.376	0.011	6
	SB-5 (7'-9')	0.104	0.0030	<Class I
	SB-8 (9'-10')	0.319	0.0093	5
	SB-10 (7'-9')	0.0385	0.0011	<Class I
	MW-8 (7'-9')	0.0371	0.0011	<Class I
	SB-11 (10'-11')	0.483	0.014	8
	SB-11 (9'-10')	0.548	0.016	9
	SB-12 (7'-9')	0.0774	0.0023	<Class I
	MW-3	N/A	0.0574	20
	MW-4	N/A	1.24	51
	MW-5	N/A	0.0735	22
	MW-7	N/A	0.0167	9
	MW-8	N/A	0.0548	19
Ethylbenzene	CS-1	15.7	0.46	<Class I
	CS-8	13.2	0.39	<Class I
	BF-1	23.4	0.68	<Class I
	BF-2	14.6	0.43	<Class I
	BF-4	18.5	0.54	<Class I
	MW-5	N/A	1.75	2

Exceeds Tier 1 SROs	Soil Saturation Limit			
	Soil Component of Groundwater Ingestion		Outdoor Inhalation	
Xylenes (total)	BF-1, BF-2		---	
Exceeds Tier 1 SROs	Soil Ingestion Exposure Route			
	Residential	Industrial/ Commercial	Construction Worker	
Benzene	CS-1, CS-7	---	---	
Exceeds Tier 1 SROs	Soil Inhalation Exposure Route			
	Residential	Industrial/ Commercial	Construction Worker	
Benzene	CS-1, CS-2, CS-5, CS-7, CS-8, CS-19, BF-5	CS-1, CS-2, CS-5, CS-7, CS-8, CS-19	CS-1, CS-2, CS-5, CS-7, CS-8, CS-19	
Xylenes (total)	---	---	CS-1, CS-2, CS-5, CS-6, CS-7, CS-8, CS-30, BF-1, BF-2, BF-3, BF-4, BF-5, SB-6 (5'-7')	
Exceeds Tier 1 SROs	Soil Component of the Groundwater Ingestion Exposure Route			
	Class I Groundwater			
Benzene	CS-1, CS-2, CS-4, CS-5, CS-6, CS-7, CS-8, CS-12, CS-19, CS-20, CS-30, BF-1, BF-2, BF-3, BF-4, BF-5, MW-4 (7'-8'), MW-5 (7'-9'), SB-5 (7'-9'), SB-8 (9'-10'), SB-10 (7'-9'), MW-8 (7'-9'), SB-11 (10'-11'), SB-11 (9'-10'), SB-12 (7'-9')			
Ethylbenzene	CS-1, CS-8, BF-1, BF-2, BF-4			
Exceeds Tier 1 SROs	Groundwater Component of the Groundwater Ingestion Exposure Route			
	Class I Groundwater			
Benzene	MW-3, MW-4, MW-5, MW-7, MW-8			
Ethylbenzene	MW-5			
Exceeds Tier 1 SROs	Indoor Inhalation Exposure Route			
	Diffusion and Advection		Diffusion Only	
	Residential	Industrial/ Commercial	Residential	Industrial/ Commercial
Benzene	MW-4	MW-4	N/A	N/A
Ethylbenzene	MW-5	MW-5	N/A	N/A

Table 1  
Summary of Analytical Results – Soil Samples  
118109 GC Real Estate, LLC  
Corrective Action Plan

Tier 1 Soil Remediation Objectives													
118109 - GC Real Estate LLC - Early Action		CS-1		CS-2		CS-3		CS-4		CS-5		CS-6	
Date of Sample Collection:		5/14/2019		5/14/2019		5/14/2019		5/14/2019		5/14/2019		5/14/2019	
Time of Sample Collection:		10:00 AM		10:05 AM		10:10 AM		10:15 AM		11:15 AM		11:20 AM	
First Environmental Lab ID:		19-2957-001		19-2957-002		19-2957-003		19-2957-004		19-2957-005		19-2957-006	
Soil Component of the Groundwater Ingestion Exposure Route													
Class I		Class II		Residential		Industrial/Commercial		Construction Worker		Industrial/Commercial		Construction Worker	
Soil Saturation Limit		Soil Component of Groundwater Ingestion		Soil Saturation Limit		Soil Component of Groundwater Ingestion		Soil Saturation Limit		Soil Component of Groundwater Ingestion		Soil Saturation Limit	
BTEX Organic Compounds (5035A/8260B)													
Date Analyzed:		5/22/2019		5/22/2019		5/21/2019		5/22/2019		5/22/2019		5/22/2019	
Units		RL		RL		RL		RL		RL		RL	
Benzene		5.0		5.0		5.0		5.0		5.0		5.0	
Toluene		5.0		5.0		5.0		5.0		5.0		5.0	
Ethylbenzene		5.0		5.0		5.0		5.0		5.0		5.0	
Total Xylenes		5.0		5.0		5.0		5.0		5.0		5.0	
Methyl-tert-butylether (MTBE)		5.0		5.0		5.0		5.0		5.0		5.0	
Solids, Total (2540B)		5.0		5.0		5.0		5.0		5.0		5.0	
Date Analyzed:		5/17/2019		5/17/2019		5/17/2019		5/17/2019		5/17/2019		5/17/2019	
Units		RL		RL		RL		RL		RL		RL	
Total Solids		80.49		84.81		83.74		91.93		83.97		83.97	
Tier 1 Soil Remediation Objectives													
118109 - GC Real Estate LLC - Early Action		CS-7		CS-8		CS-9		CS-10		CS-11		CS-12	
Date of Sample Collection:		5/14/2019		5/14/2019		5/14/2019		5/14/2019		5/15/2019		5/15/2019	
Time of Sample Collection:		12:40 PM		12:45 PM		1:00 PM		1:15 PM		9:15 AM		9:20 AM	
First Environmental Lab ID:		19-2957-007		19-2957-008		19-2957-009		19-2957-010		19-2958-001		19-2958-002	
Soil Component of the Groundwater Ingestion Exposure Route													
Class I		Class II		Residential		Industrial/Commercial		Construction Worker		Industrial/Commercial		Construction Worker	
Soil Saturation Limit		Soil Component of Groundwater Ingestion		Soil Saturation Limit		Soil Component of Groundwater Ingestion		Soil Saturation Limit		Soil Component of Groundwater Ingestion		Soil Saturation Limit	
BTEX Organic Compounds (5035A/8260B)													
Date Analyzed:		5/22/2019		5/22/2019		5/22/2019		5/22/2019		5/22/2019		5/23/2019	
Units		RL		RL		RL		RL		RL		RL	
Benzene		5.0		5.0		5.0		5.0		5.0		5.0	
Toluene		5.0		5.0		5.0		5.0		5.0		5.0	
Ethylbenzene		5.0		5.0		5.0		5.0		5.0		5.0	
Total Xylenes		5.0		5.0		5.0		5.0		5.0		5.0	
Methyl-tert-butylether (MTBE)		5.0		5.0		5.0		5.0		5.0		5.0	
Solids, Total (2540B)		5.0		5.0		5.0		5.0		5.0		5.0	
Date Analyzed:		5/17/2019		5/17/2019		5/17/2019		5/17/2019		5/17/2019		5/17/2019	
Units		RL		RL		RL		RL		RL		RL	
Total Solids		84.70		80.32		84.35		82.32		84.45		83.77	
Tier 1 Soil Remediation Objectives													
118109 - GC Real Estate LLC - Early Action		CS-13		CS-14		CS-15		CS-16		CS-17		CS-18	
Date of Sample Collection:		5/15/2019		5/15/2019		5/15/2019		5/15/2019		5/15/2019		5/15/2019	
Time of Sample Collection:		9:30 AM		9:35 AM		9:45 AM		9:55 AM		10:00 AM		10:05 AM	
First Environmental Lab ID:		19-2958-003		19-2958-004		19-2958-005		19-2958-006		19-2958-007		19-2958-008	
Soil Component of the Groundwater Ingestion Exposure Route													
Class I		Class II		Residential		Industrial/Commercial		Construction Worker		Industrial/Commercial		Construction Worker	
Soil Saturation Limit		Soil Component of Groundwater Ingestion		Soil Saturation Limit		Soil Component of Groundwater Ingestion		Soil Saturation Limit		Soil Component of Groundwater Ingestion		Soil Saturation Limit	
BTEX Organic Compounds (5035A/8260B)													
Date Analyzed:		5/22/2019		5/22/2019		5/23/2019		5/22/2019		5/22/2019		5/22/2019	
Units		RL		RL		RL		RL		RL		RL	
Benzene		5.0		5.0		5.0		5.0		5.0		5.0	
Toluene		5.0		5.0		5.0		5.0		5.0		5.0	
Ethylbenzene		5.0		5.0		5.0		5.0		5.0		5.0	
Total Xylenes		5.0		5.0		5.0		5.0		5.0		5.0	
Methyl-tert-butylether (MTBE)		5.0		5.0		5.0		5.0		5.0		5.0	
Solids, Total (2540B)		5.0		5.0		5.0		5.0		5.0		5.0	
Date Analyzed:		5/17/2019		5/17/2019		5/17/2019		5/17/2019		5/17/2019		5/17/2019	
Units		RL		RL		RL		RL		RL		RL	
Total Solids		90.43		90.10		89.11		85.96		89.98		90.65	

Analytical results in parts-per-billion (ppb) concentrations.

Analytical results in parts-per-billion (ppb) concentrations.

Exceedences of the listed SROs are indicated and bold.

Table 1  
Summary of Analytical Results – Soil Samples  
118109 GC Real Estate, LLC  
Corrective Action Plan

Tier 1 Soil Remediation Objectives												
118109 - GC Real Estate LLC - Early Action		CS-19	CS-20	CS-21	CS-22	CS-23	CS-24	Soil Component of the Groundwater Ingestion Exposure Route				
Date of Sample Collection:		5/15/2019	5/15/2019	5/15/2019	5/15/2019	5/15/2019	5/15/2019	Ingestion Exposure Route		Inhalation Exposure Route		Soil Saturation Limit
Time of Sample Collection:		10:30 AM	10:40 AM	10:45 AM	10:50 AM	11:00 AM	11:10 AM	Class I		Class II		Soil Component of Groundwater Ingestion
First Environmental Lab ID:		19-2958-009	19-2958-010	19-2958-011	19-2958-012	19-2958-013	19-2958-014	Residential	Industrial/ Commercial	Construction Worker	Industrial/ Commercial	Construction Worker
First Environmental Lab ID:		19-2958-009	19-2958-010	19-2958-011	19-2958-012	19-2958-013	19-2958-014	Residential	Industrial/ Commercial	Construction Worker	Industrial/ Commercial	Construction Worker
Date Analyzed:		5/23/2019	5/23/2019	5/22/2019	5/22/2019	5/23/2019	5/22/2019	30	170	12,000	100,000	2,300,000
Units		10,900	70.3	<5.0	<5.0	27.5	<5.0	12,000	16,000,000	410,000,000	410,000,000	410,000,000
Benzene		10,900	70.3	<5.0	<5.0	27.5	<5.0	12,000	16,000,000	410,000,000	410,000,000	410,000,000
Toluene		<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	13,000	19,000	7,800,000	200,000,000	200,000,000
Ethylbenzene		<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	13,000	19,000	7,800,000	200,000,000	200,000,000
Total Xylenes		444	<5.0	<5.0	<5.0	<5.0	<5.0	13,000	19,000	7,800,000	200,000,000	200,000,000
Methyl-tert-butylether (MTBE)		594	<5.0	<5.0	<5.0	<5.0	19.8	150,000	150,000	41,000,000	41,000,000	41,000,000
Solids, Total (2540B)		5.0	<320	<5.0	<5.0	<5.0	<320	320	320	780,000	20,000,000	2,000,000
Date Analyzed:		5/17/2019	5/17/2019	5/17/2019	5/17/2019	5/17/2019	5/17/2019	85.81	85.81	85.81	85.81	85.81
Units		86.28	86.20	94.53	95.15	84.75	85.81	85.81	85.81	85.81	85.81	85.81
Total Solids		86.28	86.20	94.53	95.15	84.75	85.81	85.81	85.81	85.81	85.81	85.81
Tier 1 Soil Remediation Objectives												
118109 - GC Real Estate LLC - Early Action		CS-25	CS-26	CS-27	CS-28	CS-29	CS-30	Soil Component of the Groundwater Ingestion Exposure Route				
Date of Sample Collection:		5/15/2019	5/15/2019	5/15/2019	5/15/2019	5/15/2019	5/15/2019	Ingestion Exposure Route		Inhalation Exposure Route		Soil Saturation Limit
Time of Sample Collection:		1:15 PM	1:30 PM	1:45 PM	2:00 PM	2:40 PM	3:00 PM	Class I		Class II		Soil Component of Groundwater Ingestion
First Environmental Lab ID:		19-2958-015	19-2958-016	19-2958-017	19-2958-018	19-2958-019	19-2958-020	Residential	Industrial/ Commercial	Construction Worker	Industrial/ Commercial	Construction Worker
First Environmental Lab ID:		19-2958-015	19-2958-016	19-2958-017	19-2958-018	19-2958-019	19-2958-020	Residential	Industrial/ Commercial	Construction Worker	Industrial/ Commercial	Construction Worker
Date Analyzed:		5/22/2019	5/22/2019	5/22/2019	5/22/2019	5/22/2019	5/23/2019	30	170	12,000	100,000	2,300,000
Units		11.8	<5.0	<5.0	<5.0	<5.0	64.5	12,000	16,000,000	410,000,000	410,000,000	410,000,000
Benzene		11.8	<5.0	<5.0	<5.0	<5.0	64.5	12,000	16,000,000	410,000,000	410,000,000	410,000,000
Toluene		<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	13,000	19,000	7,800,000	200,000,000	200,000,000
Ethylbenzene		<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	13,000	19,000	7,800,000	200,000,000	200,000,000
Total Xylenes		21.9	<5.0	<5.0	<5.0	<5.0	32.200	150,000	150,000	41,000,000	41,000,000	41,000,000
Methyl-tert-butylether (MTBE)		5.0	<5.0	<5.0	<5.0	<5.0	<320	320	320	780,000	20,000,000	2,000,000
Solids, Total (2540B)		5.0	<5.0	<5.0	<5.0	<5.0	<320	320	320	780,000	20,000,000	2,000,000
Date Analyzed:		5/20/2019	5/20/2019	5/20/2019	5/20/2019	5/20/2019	5/20/2019	89.69	89.69	89.69	89.69	89.69
Units		91.08	92.25	93.87	90.82	87.47	89.69	89.69	89.69	89.69	89.69	89.69
Total Solids		91.08	92.25	93.87	90.82	87.47	89.69	89.69	89.69	89.69	89.69	89.69
Tier 1 Soil Remediation Objectives												
118109 - GC Real Estate LLC - Early Action		BF-1	BF-2	BF-3	BF-4	BF-5	BF-6	Soil Component of the Groundwater Ingestion Exposure Route				
Date of Sample Collection:		5/14/2019	5/14/2019	5/14/2019	5/14/2019	5/14/2019	5/15/2019	Ingestion Exposure Route		Inhalation Exposure Route		Soil Saturation Limit
Time of Sample Collection:		8:30 AM	8:45 AM	9:00 AM	10:50 AM	11:30 AM	9:00 AM	Class I		Class II		Soil Component of Groundwater Ingestion
First Environmental Lab ID:		19-2957-011	19-2957-012	19-2957-013	19-2957-014	19-2957-015	19-2958-021	Residential	Industrial/ Commercial	Construction Worker	Industrial/ Commercial	Construction Worker
First Environmental Lab ID:		19-2957-011	19-2957-012	19-2957-013	19-2957-014	19-2957-015	19-2958-021	Residential	Industrial/ Commercial	Construction Worker	Industrial/ Commercial	Construction Worker
Date Analyzed:		5/22/2019	5/22/2019	5/22/2019	5/22/2019	5/22/2019	5/23/2019	30	170	12,000	100,000	2,300,000
Units		262	401	440	609	925	<25.0	12,000	16,000,000	410,000,000	410,000,000	410,000,000
Benzene		262	401	440	609	925	<25.0	12,000	16,000,000	410,000,000	410,000,000	410,000,000
Toluene		<5.0	3.010	<5.0	<5.0	2.580	<5.0	13,000	19,000	7,800,000	200,000,000	200,000,000
Ethylbenzene		<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	13,000	19,000	7,800,000	200,000,000	200,000,000
Total Xylenes		23,400	14,600	8,060	18,500	3,690	<5.0	150,000	150,000	41,000,000	41,000,000	41,000,000
Methyl-tert-butylether (MTBE)		5.0	<320	<320	<320	<320	<320	320	320	780,000	20,000,000	2,000,000
Solids, Total (2540B)		5.0	<320	<320	<320	<320	<320	320	320	780,000	20,000,000	2,000,000
Date Analyzed:		5/17/2019	5/17/2019	5/17/2019	5/17/2019	5/17/2019	5/20/2019	87.60	87.60	87.60	87.60	87.60
Units		87.60	82.25	82.35	84.25	87.12	87.60	87.60	87.60	87.60	87.60	87.60
Total Solids		87.60	82.25	82.35	84.25	87.12	87.60	87.60	87.60	87.60	87.60	87.60
Analytical results in parts-per-billion (ppb) concentrations												

Analytical results in parts-per-billion (ppb) concentrations.

Exceedences of the Tier 1 SROs are highlighted in bold.

Table 1  
Summary of Analytical Results – Soil Samples  
118109 GC Real Estate, LLC  
Corrective Action Plan

Tier 1 Soil Remediation Objectives									
118109 - GC Real Estate LLC - Stage 1		MW-1 (3-5)	MW-1 (7-9)	MW-1 (10-11)	MW-2 (1-3)	MW-2 (5-7)	MW-2 (10-11)	Soil Component of the Groundwater Ingestion Exposure Route	
Date of Sample Collection:		2/6/2020	2/6/2020	2/6/2020	2/6/2020	2/6/2020	2/6/2020	Inhalation Exposure Route	
Time of Sample Collection:		9:10 AM	9:40 AM	10:00 AM	11:00 AM	11:20 AM	11:40 AM	Soil Saturation Limit	
First Environmental Lab ID:		20-0729-001	20-0729-002	20-0729-003	20-0729-006	20-0729-007	20-0729-008	Soil Component of Groundwater Ingestion	
Date Analyzed:		2/13/2020	2/13/2020	2/14/2020	2/13/2020	2/13/2020	2/13/2020	Inhalation Exposure Route	
Units		RL	RL	RL	RL	RL	RL	Soil Saturation Limit	
Benzene		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Soil Component of Groundwater Ingestion	
Toluene		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Inhalation Exposure Route	
Ethylbenzene		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Soil Saturation Limit	
Total Xylenes		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Soil Component of Groundwater Ingestion	
Methyl-tert-butyl-ether (MTBE)		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Inhalation Exposure Route	
Solids, Total (2540B)		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Soil Saturation Limit	
Date Analyzed:		2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	Soil Component of Groundwater Ingestion	
Total Solids		75.60	87.85	89.46	91.75	94.11	84.12	Inhalation Exposure Route	
Units		---	---	---	---	---	---	Soil Saturation Limit	
Tier 1 Soil Remediation Objectives									
118109 - GC Real Estate LLC - Stage 1		MW-3 (3-5)	MW-3 (7-9)	MW-4 (3-5)	MW-4 (7-8)	MW-5 (1-3)	MW-5 (7-9)	Soil Component of the Groundwater Ingestion Exposure Route	
Date of Sample Collection:		2/6/2020	2/6/2020	2/6/2020	2/6/2020	2/7/2020	2/7/2020	Inhalation Exposure Route	
Time of Sample Collection:		12:30 PM	12:50 PM	2:10 PM	2:30 PM	8:55 AM	9:00 AM	Soil Saturation Limit	
First Environmental Lab ID:		20-0729-011	20-0729-012	20-0729-015	20-0729-016	20-0726-001	20-0726-002	Soil Component of Groundwater Ingestion	
Date Analyzed:		2/13/2020	2/13/2020	2/13/2020	2/14/2020	2/13/2020	2/14/2020	Inhalation Exposure Route	
Units		RL	RL	RL	RL	RL	RL	Soil Saturation Limit	
Benzene		5.0	<5.0	<5.0	360	<5.0	376	Soil Component of Groundwater Ingestion	
Toluene		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Inhalation Exposure Route	
Ethylbenzene		5.0	<5.0	<5.0	8.150	<5.0	4.270	Soil Saturation Limit	
Total Xylenes		5.0	<5.0	<5.0	<5.0	<5.0	1.560	Soil Component of Groundwater Ingestion	
Methyl-tert-butyl-ether (MTBE)		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Inhalation Exposure Route	
Solids, Total (2540B)		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Soil Saturation Limit	
Date Analyzed:		2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	Soil Component of Groundwater Ingestion	
Total Solids		84.46	91.5	92.28	89.75	88.74	91.51	Inhalation Exposure Route	
Units		---	---	---	---	---	---	Soil Saturation Limit	
Tier 1 Soil Remediation Objectives									
118109 - GC Real Estate LLC - Stage 1		SB-1 (1-3)	SB-1 (5-7)	SB-2 (1-3)	SB-2 (7-9)	SB-3 (1-3)	SB-3 (5-7)	Soil Component of the Groundwater Ingestion Exposure Route	
Date of Sample Collection:		2/6/2020	2/6/2020	2/6/2020	2/6/2020	2/6/2020	2/6/2020	Inhalation Exposure Route	
Time of Sample Collection:		10:20 AM	10:40 AM	12:00 PM	12:10 PM	1:20 PM	1:40 PM	Soil Saturation Limit	
First Environmental Lab ID:		20-0729-004	20-0729-005	20-0729-009	20-0729-010	20-0729-013	20-0729-014	Soil Component of Groundwater Ingestion	
Date Analyzed:		2/13/2020	2/13/2020	2/13/2020	2/13/2020	2/13/2020	2/13/2020	Inhalation Exposure Route	
Units		RL	RL	RL	RL	RL	RL	Soil Saturation Limit	
Benzene		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Soil Component of Groundwater Ingestion	
Toluene		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Inhalation Exposure Route	
Ethylbenzene		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Soil Saturation Limit	
Total Xylenes		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Soil Component of Groundwater Ingestion	
Methyl-tert-butyl-ether (MTBE)		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Inhalation Exposure Route	
Solids, Total (2540B)		5.0	<5.0	<5.0	<5.0	<5.0	<5.0	Soil Saturation Limit	
Date Analyzed:		2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	Soil Component of Groundwater Ingestion	
Total Solids		84.59	87.79	94.44	88.58	89.35	89.72	Inhalation Exposure Route	
Units		---	---	---	---	---	---	Soil Saturation Limit	
Analytical results in parts-per-billion (ppb) concentrations									

Table 1  
Summary of Analytical Results – Soil Samples  
118109 GC Real Estate, LLC  
Corrective Action Plan

Tier 1 Soil Remediation Objectives												
118109 - GC Real Estate LLC - Stage 1	Soil Component of the Groundwater Ingestion Exposure Route			Ingestion Exposure Route			Inhalation Exposure Route			Soil Saturation Limit		
	Class I			Class II			Residential	Industrial/Commercial	Construction Worker	Soil Component of Groundwater Ingestion	Soil Inhabitation	
	Class I			Class II								
	Class I			Class II								
Date of Sample Collection:	2/7/2020	2/7/2020	2/7/2020	2/7/2020	2/7/2020	2/7/2020	2/7/2020	2/7/2020	2/7/2020	2/7/2020	2/7/2020	2/7/2020
Time of Sample Collection:	10:15 AM	10:30 AM	10:45 AM	11:00 AM	11:10 AM	11:10 AM	11:00 AM	11:00 AM	11:00 AM	11:00 AM	11:00 AM	11:00 AM
First Environmental Lab ID:	20-0726-003	20-0726-004	20-0726-005	20-0726-006	20-0726-007	20-0726-008	20-0726-007	20-0726-007	20-0726-007	20-0726-007	20-0726-007	20-0726-008
BTEX Organic Compounds (5035A/8260B)												
Date Analyzed:	Units	RL	2/13/2020	2/13/2020	2/13/2020	2/13/2020	2/13/2020	2/13/2020	2/13/2020	2/13/2020	2/13/2020	2/13/2020
Benzene	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Toluene	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Ethylbenzene	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Total Xylenes	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Methyl-tert-butyl-ether (MTBE)	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Solids, Total (2540B)	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Date Analyzed:	Units	RL	2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020	2/10/2020
Total Solids	%	89.32	88.07	91.65	86.88	94.05	89.94	89.94	89.94	89.94	89.94	89.94
Tier 1 Soil Remediation Objectives												
118109 - GC Real Estate LLC - Stage 2	Soil Component of the Groundwater Ingestion Exposure Route			Ingestion Exposure Route			Inhalation Exposure Route			Soil Saturation Limit		
	Class I			Class II			Residential	Industrial/Commercial	Construction Worker	Soil Component of Groundwater Ingestion	Soil Inhabitation	
	Class I			Class II								
	Class I			Class II								
Date of Sample Collection:	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020
Time of Sample Collection:	10:00 AM	10:30 AM	11:40 AM	11:50 AM	12:15 PM	12:30 PM	12:15 PM	12:15 PM	12:15 PM	12:15 PM	12:15 PM	12:30 PM
First Environmental Lab ID:	20-6498-001	20-6498-002	20-6498-003	20-6498-004	20-6498-005	20-6498-006	20-6498-005	20-6498-005	20-6498-005	20-6498-005	20-6498-005	20-6498-006
BTEX Organic Compounds (5035A/8260B)												
Date Analyzed:	Units	RL	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020
Benzene	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Toluene	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Ethylbenzene	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Total Xylenes	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Methyl-tert-butyl-ether (MTBE)	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Solids, Total (2540B)	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Date Analyzed:	Units	RL	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020
Total Solids	%	93.96	92.39	94.04	90.91	95.74	80.50	80.50	80.50	80.50	80.50	80.50
Tier 1 Soil Remediation Objectives												
118109 - GC Real Estate LLC - Stage 2	Soil Component of the Groundwater Ingestion Exposure Route			Ingestion Exposure Route			Inhalation Exposure Route			Soil Saturation Limit		
	Class I			Class II			Residential	Industrial/Commercial	Construction Worker	Soil Component of Groundwater Ingestion	Soil Inhabitation	
	Class I			Class II								
	Class I			Class II								
Date of Sample Collection:	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020	11/13/2020
Time of Sample Collection:	12:50 PM	1:00 PM	1:30 PM	1:45 PM	1:50 PM	2:00 PM	1:50 PM	1:50 PM	1:50 PM	1:50 PM	1:50 PM	2:00 PM
First Environmental Lab ID:	20-6498-007	20-6498-008	20-6498-009	20-6498-010	20-6498-011	20-6498-012	20-6498-011	20-6498-011	20-6498-011	20-6498-011	20-6498-011	20-6498-012
BTEX Organic Compounds (5035A/8260B)												
Date Analyzed:	Units	RL	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020	11/18/2020
Benzene	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Toluene	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Ethylbenzene	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Total Xylenes	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Methyl-tert-butyl-ether (MTBE)	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Solids, Total (2540B)	µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
Date Analyzed:	Units	RL	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020	11/16/2020
Total Solids	%	94.07	88.01	95.28	87.57	92.38	89.84	89.84	89.84	89.84	89.84	89.84

Analytical results in parts-per-billion (ppb) concentrations

Analytical results in parts-per-billion (ppb) concentrations.  
Exceedences of the Tier 1 SROs are highlighted in bold.

**Table 1**  
**Summary of Analytical Results – Soil Samples**  
**118109 GC Real Estate, LLC**  
**Corrective Action Plan**

Tier 1 Soil Remediation Objectives															
118109 - GC Real Estate LLC - Stage 2		MW-9 (5'-7')	SB-11 (3'-5')	SB-11 (7'-9')	SB-11 (10'-11')	—		Inhalation Exposure Route					Soil Saturation Limit		
Date of Sample Collection:		11/13/2020	11/16/2020	11/16/2020	11/16/2020	—		Ingestion Exposure Route					Soil Saturation Limit		
Time of Sample Collection:		2:45 PM	3:00 PM	12:45 PM	1:00 PM	1:50 PM	—		Inhalation Exposure Route					Soil Saturation Limit	
First Environmental Lab ID:		20-6498-013	20-6498-014	20-6525-001	20-6525-002	20-6525-003	—		Ingestion Exposure Route					Soil Saturation Limit	
		Class I	Class II	Residential	Industrial/ Commercial	Construction Worker	Residential	Industrial/ Commercial	Construction Worker	Residential	Industrial/ Commercial	Construction Worker	Soil Component of Groundwater Ingestion	Soil Inhalation	
BTX Organic Compounds (5035A/8260B)															
Date Analyzed:		11/19/2020	11/19/2020	11/20/2020	11/20/2020	4/8	30	170	12,000	100,000	2,300,000	800	1,600	2,200	
Benzene		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Toluene		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Ethylbenzene		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Total Xylenes		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Methyl-tert-butylether (MTBE)		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Solids, Total (2540B)		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Date Analyzed:		11/16/2020	11/17/2020	11/17/2020	11/17/2020	79.80	—	—	—	—	—	—	—	—	
Total Solids		%	—	—	—	—	—	—	—	—	—	—	—	—	
118109 - GC Real Estate LLC - Stage 3															
Date of Sample Collection:		10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	
Time of Sample Collection:		12:15 PM	12:25 PM	12:35 PM	12:45 PM	11:00 AM	11:10 AM	11:10 AM	11:10 AM	11:10 AM	11:10 AM	11:10 AM	11:10 AM	11:10 AM	
First Environmental Lab ID:		21-6522-003	21-6522-004	21-6522-005	21-6522-006	21-6522-001	21-6522-002	21-6522-001	21-6522-002	21-6522-001	21-6522-002	21-6522-001	21-6522-002	21-6522-001	
BTX Organic Compounds (5035A/8260B)															
Date Analyzed:		10/7/2021	10/7/2021	10/7/2021	10/7/2021	10/7/2021	10/7/2021	10/7/2021	10/7/2021	10/7/2021	10/7/2021	10/7/2021	10/7/2021	10/7/2021	
Benzene		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Toluene		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Ethylbenzene		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Total Xylenes		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Methyl-tert-butylether (MTBE)		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Solids, Total (2540B)		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Date Analyzed:		10/7/2021	10/7/2021	10/8/2021	10/8/2021	89.44	89.44	89.44	89.44	89.44	89.44	89.44	89.44	89.44	
Total Solids		%	—	—	—	—	—	—	—	—	—	—	—	—	
118109 - GC Real Estate LLC - Stage 3															
Date of Sample Collection:		10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	10/5/2021	
Time of Sample Collection:		12:55 PM	1:05 PM	1:15 PM	1:15 PM	1:15 PM	1:15 PM	1:15 PM	1:15 PM	1:15 PM	1:15 PM	1:15 PM	1:15 PM	1:15 PM	
First Environmental Lab ID:		21-6522-007	21-6522-008	21-6522-009	21-6522-009	21-6522-009	21-6522-009	21-6522-009	21-6522-009	21-6522-009	21-6522-009	21-6522-009	21-6522-009	21-6522-009	
BTX Organic Compounds (5035A/8260B)															
Date Analyzed:		10/7/2021	10/7/2021	10/8/2021	10/8/2021	10/8/2021	10/8/2021	10/8/2021	10/8/2021	10/8/2021	10/8/2021	10/8/2021	10/8/2021	10/8/2021	
Benzene		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Toluene		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Ethylbenzene		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Total Xylenes		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Methyl-tert-butylether (MTBE)		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Solids, Total (2540B)		µg/kg	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
Date Analyzed:		10/8/2021	10/8/2021	10/8/2021	10/8/2021	88.79	88.79	88.79	88.79	88.79	88.79	88.79	88.79	88.79	
Total Solids		%	—	—	—	—	—	—	—	—	—	—	—	—	
Analytical results in parts-per-billion (ppb) concentrations															

Analytical results in parts-per-billion (ppb) concentrations. Exceedences of the *Interim* SROs published and held

**Table 1**  
**Summary of Analytical Results – Soil Samples**  
**118109 GC Real Estate, LLC**  
**Corrective Action Plan**

Tier 1 Soil Remediation Objectives																		
118109 - GC Real Estate LLC - CAP					BF-1R (13-15)	BF-2R (13-15)	BF-3R (13-15)	Soil Component of the Groundwater Ingestion Exposure Route					Inhalation Exposure Route			Soil Saturation Limit		
Date of Sample Collection:					6/2/2023	6/2/2023	6/2/2023	Class I		Class II	Residential	Industrial/ Commercial	Construction Worker	Residential	Industrial/ Commercial	Construction Worker	Soil Component of Groundwater Ingestion	Soil Inhalation
Time of Sample Collection:					11:00 AM	11:30 AM	12:00 PM											
First Environmental Lab ID:					23-4572-001	23-4572-002	23-4572-003											
BTEX Organic Compounds (5035A-8260B)																		
Date Analyzed:					6/12/2023	6/8/2023	6/8/2023											
Benzene	Units	RL	%		8,500	<50	<50	30	170		12,000	100,000	2,300,000	800	1,600	2,200	580,000	800,000
Toluene	µg/kg	50	152		<50	<50	<50	12,000	29,000		16,000,000	410,000,000	410,000,000	650,000	650,000	43,000	290,000	380,000
Ethylbenzene	µg/kg	50	2,500		<50	<50	<50	13,000	19,000		7,800,000	200,000,000	20,000,000	400,000	400,000	55,000	350,000	580,000
Xylenes	µg/kg	50	4,970		<50	<50	<50	150,000	150,000		16,000,000	410,000,000	41,000,000	320,000	320,000	5,600	110,000	280,000
Methyl-ter-butylalcohol (MTBE)	µg/kg	50	<320		<50	<50	<50	320	320		780,000	20,000,000	2,000,000	8,800,000	8,800,000	140,000	8,400,000	1,200,000,000
Solids, Total (2540B)																		
Date Analyzed:					6/5/2023	6/5/2023	6/5/2023											
Units					RL	---	---											
Total Solids					%	78.04	83.24											
Analytical results in parts-per-billion (ppb) concentrations.																		
Exceedence of the Tier 1 Soil Saturation Limit and/or																		

Analytical results in parts-per-billion (ppb) concentrations.

Exceedences of the Tier 1 SROs highlighted and bold

**Table 2**  
**Summary of Analytical Results - Groundwater Samples**  
**118109 - GC Real Estate LLC**  
**Corrective Action Plan**

118109 - GC Real Estate LLC - Stage 1				Tier 1 Groundwater Remediation Objectives							
Date of Sample Collection:				MW-1	MW-2	MW-3	MW-4	MW-5	Class I	Class II	Indoor Inhalation Exposure Route
Time of Sample Collection:				12:00 PM	12:15 PM	12:30 PM	1:00 PM	1:20 PM			Diffusion and Advection
First Environmental Lab ID:				20-0990-001	20-0990-002	20-0990-003	20-0990-004	20-0990-005			Residential
BTEX Organic Compounds (5035A/8260B)											
Date Analyzed:		Units	RL	2/25/2020	2/25/2020	2/27/2020	2/27/2020	2/25/2020			
Benzene		µg/L	5.0	<5.0	<5.0	57.4	1,240	73.5	5.0	25	---
Toluene		µg/L	5.0	<5.0	<5.0	<5.0	11.2	19.6	1,000	2,500	111
Ethylbenzene		µg/L	5.0	41.3	<5.0	102	284	1,750	700	1,000	530,000
Total Xylenes		µg/L	5.0	36.7	<5.0	<5.0	96.3	3,780	10,000	10,000	370
Methyl-tert-butylether (MTBE)		µg/L	5.0	<5.0	<5.0	<5.0	12.6	12	70	70	30,000
											1,900,000
											6,800,000
118109 - GC Real Estate LLC - Stage 2											
Date of Sample Collection:				MW-7	MW-8	MW-9	Tier 1 Groundwater Remediation Objectives				
Time of Sample Collection:				12/4/2020	12/4/2020	12/4/2020	Indoor Inhalation Exposure Route				
First Environmental Lab ID:				20-6877-001	20-6877-002	20-6877-003	Diffusion and Advection				
First Environmental Lab ID:				20-6877-001	20-6877-002	20-6877-003	Residential				
First Environmental Lab ID:				20-6877-001	20-6877-002	20-6877-003	Industrial/ Commercial				
BTEX Organic Compounds (5035A/8260B)											
Date Analyzed:		Units	RL	12/8/2020	12/8/2020	12/8/2020					
Benzene		µg/L	5.0	16.7	54.8	<5.0	5.0				
Toluene		µg/L	5.0	<5.0	<5.0	<5.0	1,000				
Ethylbenzene		µg/L	5.0	<5.0	30.8	13.3	700				
Total Xylenes		µg/L	5.0	9.6	<5.0	<5.0	10,000				
Methyl-tert-butylether (MTBE)		µg/L	5.0	<5.0	<5.0	<5.0	70				
							25				
							111				
							530,000				
							370				
							30,000				
							1,900,000				
							6,800,000				

**Exceeds Class I GROs or Appendix B, Table H**

Diffusion and Advection Objectives Based on 35 IAC Part 742 Appendix B Table H.

**Table 2**  
**Summary of Analytical Results - Groundwater Samples**  
**118109 - GC Real Estate LLC**  
**Corrective Action Plan**

118109 - GC Real Estate LLC - Stage 3				MW-6	MW-11	GMW-7	GMW-8	GMW-9	Tier 1 Groundwater Remediation Objectives			
Date of Sample Collection:				10/26/2021	10/26/2021	10/26/2021	10/26/2021	10/26/2021	Indoor Inhalation Exposure Route			
Time of Sample Collection:				11:00 AM	11:30 AM	1:00 PM	2:15 PM	2:00 PM	Diffusion and Advection			
First Environmental Lab ID:				21-7108-001	21-7108-002	21-7108-003	21-7108-004	21-7108-005	Industrial/Commercial			
BTEX Organic Compounds (5035A/8260B)												
Date Analyzed:		Units	RL	10/29/2021	10/29/2021	10/29/2021	10/29/2021	10/29/2021	Class I		Class II	
Benzene		µg/L	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	5.0	25	---	
Toluene		µg/L	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	1,000	2,500	111	
Ethylbenzene		µg/L	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	700	1,000	530,000	
Total Xylenes		µg/L	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	10,000	10,000	370	
Methyl-tert-butylether (MTBE)		µg/L	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	70	70	30,000	
										1,900,000	6,800,000	
118109 - GC Real Estate LLC - Stage 3												
Date of Sample Collection:				10/26/2021	10/26/2021	10/26/2021			Class I		Class II	
Time of Sample Collection:				1:45 PM	1:30 PM	12:00 PM			Diffusion and Advection		Indoor Inhalation Exposure Route	
First Environmental Lab ID:				21-7108-006	21-7108-007	21-7108-008			Residential		Industrial/Commercial	
BTEX Organic Compounds (5035A/8260B)												
Date Analyzed:		Units	RL	10/29/2021	10/29/2021	10/29/2021	10/29/2021	10/29/2021	Class I		Class II	
Benzene		µg/L	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	5.0	25	---	
Toluene		µg/L	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	1,000	2,500	111	
Ethylbenzene		µg/L	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	700	1,000	530,000	
Total Xylenes		µg/L	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	10,000	10,000	370	
Methyl-tert-butylether (MTBE)		µg/L	5.0	<5.0	<5.0	<5.0	<5.0	<5.0	70	70	30,000	
										1,900,000	6,800,000	

Diffusion and Advection Objectives Based on 35 IAC Part 742 Appendix B Table H.

**Table 3**  
**Summary of Analytical Results - Indoor Inhalation Exposure Route**  
**118109 - GC Real Estate**  
**Corrective Action Plan**

Sample ID :		MW-4	MW-5	Tier 1 Groundwater Remediation Objectives for Indoor Inhalation Exposure Route			
Laboratory ID :		20-0990-004	20-0990-005				
Date Collected :		02/21/20	02/21/20				
CAS No.	Analyte	Result (ug/L)	Result (ug/L)	Diffusion and Advection (mg/L)		Diffusion Only (mg/L)	
71-43-2	Benzene	1.24	0.0735	Residential	Industrial/ Commercial	Residential	Industrial/ Commercial
108-88-3	Toluene	0.0112	0.0196	530	530	530	530
100-41-4	Ethylbenzene	0.284	1.75	0.37	1.4	1.3	8.1
1330-20-7	Xylenes, Total	0.0963	3.78	30	93	96	110
1634-04-4	MTBE	0.0126	0.012	1,900	6,800	30,000	51,000
Sample ID :		VP-1	VP-2	Tier 1 Soil Gas Remediation Objectives for Indoor Inhalation Exposure Route			
Laboratory ID :		23-4574-001	23-4574-002				
Date Collected :		06/02/23	06/02/23				
CAS No.	Analyte	Result (mg/m <sup>3</sup> )	Result (mg/m <sup>3</sup> )	Diffusion & Advection (mg/m <sup>3</sup> )		Diffusion Only (mg/m <sup>3</sup> )	
71-43-2	Benzene	1.8	0.0091	Residential	Industrial / Commercial	Residential	Industrial / Commercial
108-88-3	Toluene	<0.81	0.013	6,200	40,000	140,000	140,000
100-41-4	Ethylbenzene	<0.94	0.017	1.3	9.3	150	1,100
1330-20-7	Xylenes, Total	<2.8	0.074	140	840	17,000	49,000
1634-04-4	MTBE	<0.78	<0.0026	3,700	24,000	420,000	1,200,000
67-63-0	Isopropyl Alcohol	<2.7	<0.0090	---	---	---	---

## Illinois Environmental Protection Agency Leaking Underground Storage Tank Program RBCA Input Parameters for Use with Tier 2 Calculations

### A. Site Identification

IEMA Incident # (6- or 8-digit): 20190483, 20050170 IEPA LPC # (10-digit): 0894076105

Site Name: GC Real Estate, LLC.

Site Address (not a P.O. Box): 1125 Aurora Avenue

City: Aurora County: Kane Zip Code: 60505

Leaking UST Technical File

### B. Tier 2 Calculation Information

Equation(s) Used (ex: R12, R14, R26): R26

Contact Information for Individual Who Performed Calculations: Jeff Ogden, Senior Project

Manager, Eagle Environmental Consultants, LLC Phone: (630) 940-2540

Land Use: Not Applicable Soil Type: Sand

Groundwater: ☒ Class I ☐ Class II

Mass Limit: ☐ Yes ☒ No If Yes, then Specify Acreage: ☐ 0.5 ☐ 1 ☐ 2 ☐ 5 ☐ 10 ☐ 30

Result from S18/S28 used in R26? ☒ Yes ☐ No Specify  $C_{source}$  from S18/S28 \_\_\_\_\_ mg/L

- Mass Limit Acreage other than defaults must always be rounded up.
- Failure to use site-specific parameters where allowed could affect payment from the Underground Storage Tank Fund.
- Maps depicting source width, plume dimensions, distance, etc. must also be submitted.
- Inputs must be submitted in the designated unit.

Symbol		Unit
AT <sub>c</sub>	= 70	yr
AT <sub>n</sub>	=	yr
BW	= 70	kg
C <sub>source</sub>	= see page 3	mg/L
C <sub>(x)</sub>	= see page 3	mg/L
C <sub>(x)</sub> /C <sub>source</sub>	=	unitless

Symbol		Unit
d	=	cm
D <sup>air</sup>	=	cm <sup>2</sup> /s
D <sup>water</sup>	=	cm <sup>2</sup> /s
D <sub>s</sub> <sup>eff</sup>	=	cm <sup>2</sup> /s
ED	=	yr
EF	=	d/yr

Symbol		Unit	Symbol		Unit
erf	=	unitless	RAF <sub>d</sub> (PNAs)	= 0.05	unitless
f <sub>oc</sub>	=	g/g	RAF <sub>d</sub> (inorganics)	= 0	unitless
GW <sub>comp</sub>	=	mg/L	RAF <sub>0</sub>	= 1.0	unitless
GW <sub>source</sub>	=	mg/L	RBSL <sub>air</sub> (carcinogenic)	=	µg/m <sup>3</sup>
H'	=	cm <sup>3</sup> <sub>water</sub> /cm <sup>3</sup> <sub>air</sub>	RBSL <sub>air</sub> (noncarcinogenic)	=	µg/m <sup>3</sup>
i	= 0.03	cm/cm	RfD <sub>i</sub>	=	mg/kg-d
I	= 30	cm/yr	RfD <sub>0</sub>	=	mg/kg-d
IR <sub>air</sub>	= 20	m <sup>3</sup> /d	SA	= 3,160	cm <sup>2</sup> /d
IR <sub>soil</sub>	=	mg/d	S <sub>d</sub>	= 200	cm
IR <sub>w</sub>	=	L/d	S <sub>w</sub>	= 4,965.19	cm
K	= 1.841	cm/d for R15, R19, R26; cm/yr for R24	SF <sub>i</sub>	=	(mg/kg-d) <sup>-1</sup>
K <sub>oc</sub>	=	cm <sup>3</sup> /g or L/kg	SF <sub>0</sub>	=	(mg/kg-d) <sup>-1</sup>
k <sub>s</sub> (non-ionizing organics)	=	cm <sup>3</sup> <sub>water</sub> /g <sub>soil</sub>	THQ	= 1	unitless
k <sub>s</sub> (ionizing organics)	=	cm <sup>3</sup> <sub>water</sub> /g <sub>soil</sub>	TR	=	unitless
k <sub>s</sub> (inorganics)	=	cm <sup>3</sup> <sub>water</sub> /g <sub>soil</sub>	U	=	cm/d
L <sub>s</sub>	= 100	cm	U <sub>air</sub>	= 225	cm/s
LF <sub>sw</sub>	=	(mg/L <sub>water</sub> ) / (mg/kg <sub>soil</sub> )	U <sub>gw</sub>	=	cm/yr
M	= 0.5	mg/cm <sup>2</sup>	VF <sub>p</sub>	=	kg/m <sup>3</sup>
Pe	= 6.9 •10 <sup>-14</sup>	g/cm <sup>2</sup> -s	VF <sub>samb</sub>	=	(mg/m <sup>3</sup> <sub>air</sub> )/mg/kg <sub>soil</sub> or kg/m <sup>3</sup>
RAF <sub>d</sub>	= 0.5	unitless	VF <sub>ss</sub>	=	kg/m <sup>3</sup>

Symbol		Unit	Symbol		Unit
W	=	cm	$\theta_{as}$	=	$\text{cm}^3_{\text{air}}/\text{cm}^3_{\text{soil}}$
w	=	$\text{g}_{\text{water}}/\text{g}_{\text{soil}}$	$\theta_{ws}$	=	$\text{cm}^3_{\text{water}}/\text{cm}^3_{\text{soil}}$
X	=	see below	$\theta_T$	=	0.32 $\text{cm}^3/\text{cm}^3_{\text{soil}}$
$\alpha_x$	=	cm	$\lambda$	=	0.0009 $\text{d}^{-1}$
$\alpha_y$	=	cm	$\pi$	=	3.1416
$\alpha_z$	=	cm	$\rho_b$	=	$\text{g}/\text{cm}^3$
$\delta_{\text{air}}$	=	200	$\rho_w$	=	1 $\text{g}/\text{cm}^3$
$\delta_{\text{gw}}$	=	200	$\tau$	=	$9.46 \cdot 10^8$ s

Equation	Result	Unit(s)
R1	=	mg/kg
R2	=	mg/kg
R7	=	mg/kg
R8	=	mg/kg
R12	=	mg/kg
R25	=	mg/L

## Csource Values: (mg/L)

CS-1 = 0.386    SB-12 (7'-9') = 0.0023  
 CS-2 = 0.225  
 CS-4 = 0.0015  
 CS-5 = 0.135  
 CS-6 = 0.020  
 CS-7 = 0.702  
 CS-8 = 0.228  
 CS-12 = 0.0039  
 CS-19 = 0.319  
 CS-20 = 0.0021  
 CS-30 = 0.0019  
 BF-1 = 0.0077  
 BF-2 = 0.012  
 BF-3 = 0.013  
 BF-4 = 0.018  
 BF-5 = 0.027  
 MW-4 (7'-8') = 0.011  
 MW-5 (7'-9') = 0.011  
 SB-5 (7'-9') = 0.0030  
 SB-8 (9'-10') = 0.0093  
 SB-10 (7'-9') = 0.0011  
 MW-8 (7'-9') = 0.0011  
 SB-11 (10'-11') = 0.014  
 SB-11 (9'-10') = 0.016

**Maximum Predicted Extent of Groundwater Impact (X):**  
(feet from point source)

CS-1 = 39	SB-12 (7'-9') = <Class I	BF-2 = 6
CS-2 = 33		BF-3 = 7
CS-4 = <Class I		BF-4 = 10
CS-5 = 28		BF-5 = 13
CS-6 = 10		MW-4 (7'-8') = 6
CS-7 = 45		MW-5 (7'-9') = 6
CS-8 = 33		SB-5 (7'-9') = <Class I
CS-12 = <Class I		SB-8 (9'-10') = 5
CS-19 = 37		SB-10 (7'-9') = <Class I
CS-20 = <Class I		MW-8 (7'-9') = <Class I
CS-30 = <Class I		SB-11 (10'-11') = 8
BF-1 = 3		SB-11 (9'-10') = 9

**RBCA Equation R26**  
**Dissolved Hydrocarbon Concentration Along Centerline**  
**Maximum Predicted Extent of Groundwater Impact Modeling**  
**Groundwater Component of the Groundwater Ingestion Exposure Route**  
1125 Aurora Avenue  
Aurora

**Input Parameters Used in the Solution of Equation R26**

Parameter	Value	Description
First Order Degradation Constant ( $\lambda$ )	Benzene: 0.0009/day Ethylbenzene: 0.003/day	Default Value (Appendix C, Table E)
Aquifer Hydraulic Conductivity (K)	2.131E-05 cm/sec	Site specific value as provided in approved SICR dated September 2, 2021
Hydraulic Gradient (i)	0.03 cm/cm	Site specific value as provided in approved SICR dated February 7, 2022
Total Soil Porosity ( $\theta_r$ )	0.32 cm <sup>3</sup> /cm <sup>3</sup>	Default for sand
Source Width Perpendicular to Groundwater Flow in the Horizontal Plane ( $S_w$ )	4,965.19 cm	Site specific value as provided in approved SICR dated February 7, 2022
Source Width Perpendicular to Groundwater Flow in the Vertical Plane ( $S_d$ )	200 cm	Default Value Appendix C, Table D
Tier 1 Groundwater Remediation Objective for Class I groundwater at the point of human exposure ( $C_x$ )	Benzene: 0.005 mg/L Ethylbenzene: 0.7 mg/L	Appendix B, Table E

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	CS-1
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	05/14/2019
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009/\text{day}$

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_T$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity  $A_x$ =  cm

Transverse dispersivity  $A_y$ =  cm

Vertical dispersivity  $A_z$ =  cm

Specific discharge  $U$ =  cm/day

$Sw/(4*\text{SQRT}(A_y*X))$   $B$ =

$Sd/(2*\text{SQRT}(A_z*X))$   $C$ =

Error function  $\text{erf}(B)$ =  To determine error function values,

Error function  $\text{erf}(C)$ =  see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual  $\text{erf}(B)$   Actual  $\text{erf}(C)$ =

**Solutions**

$C_{(x)}$   
 mg/l

Computation of  $\text{erf}(x)$

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	5.854593479	1.217485691
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.342710731	0.714879331
$\text{erf}(x)$ =	1	0.914891557

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
Site Name & Location:	1125 Aurora Avenue Aurora	Sample Location:	CS-2
LUST Incident Number(s):	20190483, 20050170	Sample Date:	05/14/2019
Exposure Pathway:	Groundwater Component of Groundwater Ingestion		
Groundwater Classification:	Class I	Analyte:	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_T$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity  $A_x$ =  cm

Transverse dispersivity  $A_y$ =  cm

Vertical dispersivity  $A_z$ =  cm

Specific discharge  $U$ =  cm/day

$Sw/(4*\sqrt{A_y*X})$   $B$ =

$Sd/(2*\sqrt{A_z*X})$   $C$ =

Error function  $erf(B)$ =  To determine error function values,

Error function  $erf(C)$ =  see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual  $erf(B)$   Actual  $erf(C)$

**Solutions**

$C_{(x)}$   
 mg/l

Computation of  $erf(x)$

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	6.863384971	1.427267841
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.307845394	0.681403033
$erf(x)$ =	1	0.956456921

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
Site Name & Location:	1125 Aurora Avenue Aurora	Sample Location:	CS-5
LUST Incident Number(s):	20190483, 20050170	Sample Date:	05/14/2019
Exposure Pathway:	Groundwater Component of Groundwater Ingestion		
Groundwater Classification:	Class I	Analyte:	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="83.2"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="27.7"/> cm	
Vertical dispersivity	Az=	<input type="text" value="4.2"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\sqrt{Ay*X})$	B=	<input type="text" value="8.2"/>	
$Sd/(2*\sqrt{Az*X})$	C=	<input type="text" value="1.7"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values, see F46 & K46 in the linear interpolation section.
Error function	erf(C)=	<input type="text" value="1.0"/>	

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)=  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	8.170696394	1.699128383
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.271986918	0.64241782
erf(x)=	1	0.98373573

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	CS-6
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	05/14/2019
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="30.2"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="10.1"/> cm	
Vertical dispersivity	Az=	<input type="text" value="1.5"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\sqrt{Ay*X})$	B=	<input type="text" value="22.5"/>	
$Sd/(2*\sqrt{Az*X})$	C=	<input type="text" value="4.7"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)=  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

**Computation of erf(x)**

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	22.5313143	4.685475237
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.119316678	0.394489769
erf(x)=	1	1

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	CS-7
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	05/14/2019
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  in/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="135.9"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="45.3"/> cm	
Vertical dispersivity	Az=	<input type="text" value="6.8"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\sqrt{Ay*X})$	B=	<input type="text" value="5.0"/>	
$Sd/(2*\sqrt{Az*X})$	C=	<input type="text" value="1.0"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values, see F46 & K46 in the linear interpolation section.
Error function	erf(C)=	<input type="text" value="0.9"/>	

Actual B value=	<input type="text" value="5.0"/>	Actual C value=	<input type="text" value="1.0"/>
Automatic calculations : Actual erf(B)	<input type="text" value="1.0"/>	Actual erf(C)=	<input type="text" value="0.9"/>

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	5.00134555	1.040049436
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.379018119	0.745872933
erf(x)=	1	0.858668783

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
Site Name & Location:	1125 Aurora Avenue Aurora	Sample Location:	CS-8
LUST Incident Number(s):	20190483, 20050170	Sample Date:	05/14/2019
Exposure Pathway:	Groundwater Component of Groundwater Ingestion	Analyte: Benzene	
Groundwater Classification:	Class I		

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_T$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="99.7"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="33.2"/> cm	
Vertical dispersivity	Az=	<input type="text" value="5.0"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\sqrt{Ay*X})$	B=	<input type="text" value="6.8"/>	
$Sd/(2*\sqrt{Az*X})$	C=	<input type="text" value="1.4"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)=  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

**Computation of erf(x)**

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	6.821407081	1.418538374
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.309154155	0.682733411
erf(x)=	1	0.955156287

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b> CS-19 <b>Sample Date:</b> 05/15/2019
<b>LUST Incident Number(s):</b>	20190483, 20050170	
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion	
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b> Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="110.0"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="36.7"/> cm	
Vertical dispersivity	Az=	<input type="text" value="5.5"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4 \cdot \sqrt{Ay \cdot X})$	B=	<input type="text" value="6.2"/>	
$Sd/(2 \cdot \sqrt{Az \cdot X})$	C=	<input type="text" value="1.3"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="0.9"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	6.178947688	1.284936422
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.330669431	0.703762586
erf(x)=	1	0.930809715

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCE EQUATION R26**

Site Details		Sample Details	
Site Name & Location:	1125 Aurora Avenue Aurora	Sample Location:	BF-1
LUST Incident Number(s):	20190483, 20050170	Sample Date:	05/14/2019
Exposure Pathway:	Groundwater Component of Groundwater Ingestion	Analyte: Benzene	
Groundwater Classification:	Class I		

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009/\text{day}$

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  in/in

Total soil porosity ( $\theta_r$ )=   $\text{cm}^3/\text{cm}^3_{\text{sol}}$

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	$A_x$ =	<input type="text" value="8.5"/> cm	
Transverse dispersivity	$A_y$ =	<input type="text" value="2.8"/> cm	
Vertical dispersivity	$A_z$ =	<input type="text" value="0.4"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\text{SQRT}(A_y*X))$	B=	<input type="text" value="79.7"/>	
$Sd/(2*\text{SQRT}(A_z*X))$	C=	<input type="text" value="16.6"/>	
Error function	$\text{erf}(B)$ =	<input type="text" value="1.0"/>	To determine error function values, see F46 & K46 in the linear interpolation section.
Error function	$\text{erf}(C)$ =	<input type="text" value="1.0"/>	

Actual B value=  Actual C value=

Automatic calculations : Actual  $\text{erf}(B)$   Actual  $\text{erf}(C)$ =

**Solutions**

$C_{(x)}$   
 mg/l

Computation of  $\text{erf}(x)$

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	79.66428984	16.56650173
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.036904029	0.155592657
$\text{erf}(x)$ =	1	1

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	BF-2
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	05/14/2019
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_T$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="18.2"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="6.1"/> cm	
Vertical dispersivity	Az=	<input type="text" value="0.9"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\sqrt{Ay*X})$	B=	<input type="text" value="37.4"/>	
$Sd/(2*\sqrt{Az*X})$	C=	<input type="text" value="7.8"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	37.36348602	7.769883559
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.075529012	0.282060021
erf(x)=	1	1

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBGA EQUATION R26**

Site Details		Sample Details	
Site Name & Location:	1125 Aurora Avenue Aurora	Sample Location:	BF-3
LUST Incident Number(s):	20190483, 20050170	Sample Date:	05/14/2019
Exposure Pathway:	Groundwater Component of Groundwater Ingestion	Analyte: Benzene	
Groundwater Classification:	Class I		

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft ==  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009/\text{day}$

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="20.1"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="6.7"/> cm	
Vertical dispersivity	Az=	<input type="text" value="1.0"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\sqrt{Ay*X})$	B=	<input type="text" value="33.9"/>	
$Sd/(2*\sqrt{Az*X})$	C=	<input type="text" value="7.0"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values, see F46 & K46 in the linear interpolation section.
Error function	erf(C)=	<input type="text" value="1.0"/>	

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26  
Maximum error in computation =  $1.5 \times 10^{-7}$

x=	33.8996978	7.049575205
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.082608859	0.302171578
erf(x)=	1	1

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	BF-4
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	05/14/2019
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  in/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="27.6"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="9.2"/> cm	
Vertical dispersivity	Az=	<input type="text" value="1.4"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*SQRT(Ay*X))$	B=	<input type="text" value="24.6"/>	
$Sd/(2*SQRT(Az*X))$	C=	<input type="text" value="5.1"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	24.59316555	5.114245297
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.110417906	0.373778505
erf(x)=	1	1

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	BF-5
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	05/14/2019
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity  $A_x$ =  cm

Transverse dispersivity  $A_y$ =  cm

Vertical dispersivity  $A_z$ =  cm

Specific discharge  $U$ =  cm/day

$Sw/(4*\sqrt{A_y*X})$   $B$ =

$Sd/(2*\sqrt{A_z*X})$   $C$ =

Error function  $erf(B)$ =  To determine error function values,

Error function  $erf(C)$ =  see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual  $erf(B)$   Actual  $erf(C)$ =

**Solutions**

$C_{(x)}$   
 mg/l

Computation of  $erf(x)$

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	17.98871061	3.740822971
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.145075945	0.449345241
$erf(x)$ =	1	0.999999878

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
Site Name & Location:	1125 Aurora Avenue Aurora	Sample Location:	MW-4 (7'-8')
LUST Incident Number(s):	20190483, 20050170	Sample Date:	02/06/2020
Exposure Pathway:	Groundwater Component of Groundwater Ingestion	Analyte: Benzene	
Groundwater Classification:	Class I		

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009/\text{day}$

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="16.2"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="5.4"/> cm	
Vertical dispersivity	Az=	<input type="text" value="0.8"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\text{SQRT}(Ay*X))$	B=	<input type="text" value="42.1"/>	
$Sd/(2*\text{SQRT}(Az*X))$	C=	<input type="text" value="8.8"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	42.08679463	8.752114122
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.067625784	0.258590727
erf(x)=	1	1

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	MW-5 (7'-9')
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	02/07/2020
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009/\text{day}$

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="16.2"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="5.4"/> cm	
Vertical dispersivity	Az=	<input type="text" value="0.8"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\text{SQRT}(Ay*X))$	B=	<input type="text" value="42.1"/>	
$Sd/(2*\text{SQRT}(Az*X))$	C=	<input type="text" value="8.8"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)=  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	42.08679463	8.752114122
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.067625784	0.258590727
erf(x)=	1	1

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	SB-8 (9'-10')
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	11/13/2020
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{\text{source}}$ )= 0.0093 mg/L

Distance along centerline of the plume coming from the source (X)= 4.1 ft = 124.97 cm

First order degradation constant ( $\lambda$ )= 0.0009 /day if benzene,  $\lambda=0.0009/\text{day}$

Aquifer hydraulic conductivity (K)= 2.131E-05 cm/sec = 1.841 cm/day

Hydraulic gradient (i)= 0.03 m/m

Total soil porosity ( $\theta_p$ )= 0.32  $\text{cm}^3/\text{cm}^3_{\text{soil}}$

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )= 162.9 ft = 4,965.19 cm

Source width perpendicular to GW flow direction in vertical plane ( $S_v$ )= 6.56 ft = 200 cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	$A_x$ =	<span style="border: 1px solid black; padding: 2px;">12.5</span> cm	
Transverse dispersivity	$A_y$ =	<span style="border: 1px solid black; padding: 2px;">4.2</span> cm	
Vertical dispersivity	$A_z$ =	<span style="border: 1px solid black; padding: 2px;">0.6</span> cm	
Specific discharge	U=	<span style="border: 1px solid black; padding: 2px;">0.2</span> cm/day	
$Sw/(4*\text{SQRT}(A_y*X))$	B=	<span style="border: 1px solid black; padding: 2px;">54.4</span>	
$Sd/(2*\text{SQRT}(A_z*X))$	C=	<span style="border: 1px solid black; padding: 2px;">11.3</span>	
Error function	$\text{erf}(B)$ =	<span style="border: 1px solid black; padding: 2px;">1.0</span>	To determine error function values,
Error function	$\text{erf}(C)$ =	<span style="border: 1px solid black; padding: 2px;">1.0</span>	see F46 & K46 in the linear interpolation section.

Actual B value=	<span style="border: 1px solid black; padding: 2px;">54.4</span>	Actual C value=	<span style="border: 1px solid black; padding: 2px;">11.3</span>
Automatic calculations : Actual $\text{erf}(B)$	<span style="border: 1px solid black; padding: 2px;">1.0</span>	Actual $\text{erf}(C)$ =	<span style="border: 1px solid black; padding: 2px;">1.0</span>

**Solutions**

$C_{(x)}$   
0.005 mg/l

Computation of  $\text{erf}(x)$

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	54.40488086	11.3137085
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.053127751	0.212482487
$\text{erf}(x)$ =	1	1

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	SB-11 (10'-11')
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	11/16/2020
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009/\text{day}$

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=   $\text{cm}^3/\text{cm}^3_{\text{sol}}$

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="21.6"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="7.2"/> cm	
Vertical dispersivity	Az=	<input type="text" value="1.1"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\text{SQRT}(Ay*X))$	B=	<input type="text" value="31.4"/>	
$Sd/(2*\text{SQRT}(Az*X))$	C=	<input type="text" value="6.5"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	31.41690303	6.533268288
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.088559073	0.318446942
erf(x)=	1	1

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	SB-11 (9'-10')
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	10/05/2021
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009/\text{day}$

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=   $\text{cm}^3/\text{cm}^3_{\text{soil}}$

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="24.8"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="8.3"/> cm	
Vertical dispersivity	Az=	<input type="text" value="1.2"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\text{SQRT}(Ay*X))$	B=	<input type="text" value="27.4"/>	
$Sd/(2*\text{SQRT}(Az*X))$	C=	<input type="text" value="5.7"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)=  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	27.36932657	5.691558877
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.100341686	0.349100573
erf(x)=	1	1

## Illinois Environmental Protection Agency Leaking Underground Storage Tank Program RBCA Input Parameters for Use with Tier 2 Calculations

### A. Site Identification

IEMA Incident # (6- or 8-digit): 20190483, 20050170 IEPA LPC # (10-digit): 0894076105

Site Name: GC Real Estate, LLC.

Site Address (not a P.O. Box): 1125 Aurora Avenue

City: Aurora County: Kane Zip Code: 60505

Leaking UST Technical File

### B. Tier 2 Calculation Information

Equation(s) Used (ex: R12, R14, R26): R26

Contact Information for Individual Who Performed Calculations: Jeff Ogden, Senior Project

Manager, Eagle Environmental Consultants, LLC Phone: (630) 940-2540

Land Use: Not Applicable Soil Type: Sand

Groundwater: ☒ Class I ☐ Class II

Mass Limit: ☐ Yes ☒ No If Yes, then Specify Acreage: ☐ 0.5 ☐ 1 ☐ 2 ☐ 5 ☐ 10 ☐ 30

Result from S18/S28 used in R26? ☐ Yes ☒ No Specify  $C_{\text{source}}$  from S18/S28                      mg/L

- Mass Limit Acreage other than defaults must always be rounded up.
- Failure to use site-specific parameters where allowed could affect payment from the Underground Storage Tank Fund.
- Maps depicting source width, plume dimensions, distance, etc. must also be submitted.
- Inputs must be submitted in the designated unit.

Symbol		Unit	Symbol		Unit	
AT <sub>c</sub>	=	70	yr	d	=	cm
AT <sub>n</sub>	=		yr	D <sup>air</sup>	=	cm <sup>2</sup> /s
BW	=	70	kg	D <sup>water</sup>	=	cm <sup>2</sup> /s
C <sub>source</sub>	=	see page 3	mg/L	D <sub>s</sub> <sup>eff</sup>	=	cm <sup>2</sup> /s
C <sub>(x)</sub>	=	see page 3	mg/L	ED	=	yr
C <sub>(x)</sub> /C <sub>source</sub>	=		unitless	EF	=	d/yr

Symbol		Unit	Symbol		Unit
erf	=	unitless	RAF <sub>d</sub> (PNAs)	= 0.05	unitless
f <sub>oc</sub>	=	g/g	RAF <sub>d</sub> (inorganics)	= 0	unitless
GW <sub>comp</sub>	=	mg/L	RAF <sub>0</sub>	= 1.0	unitless
GW <sub>source</sub>	=	mg/L	RBSL <sub>air</sub> (carcinogenic)	=	µg/m <sup>3</sup>
H'	=	cm <sup>3</sup> <sub>water</sub> /cm <sup>3</sup> <sub>air</sub>	RBSL <sub>air</sub> (noncarcinogenic)	=	µg/m <sup>3</sup>
i	= 0.03	cm/cm	RfD <sub>i</sub>	=	mg/kg-d
I	= 30	cm/yr	RfD <sub>0</sub>	=	mg/kg-d
IR <sub>air</sub>	= 20	m <sup>3</sup> /d	SA	= 3,160	cm <sup>2</sup> /d
IR <sub>soil</sub>	=	mg/d	S <sub>d</sub>	= 200	cm
IR <sub>w</sub>	=	L/d	S <sub>w</sub>	= 6,681.22	cm
K	= 1.841	cm/d for R15, R19, R26; cm/yr for R24	SF <sub>i</sub>	=	(mg/kg-d) <sup>-1</sup>
K <sub>oc</sub>	=	cm <sup>3</sup> /g or L/kg	SF <sub>0</sub>	=	(mg/kg-d) <sup>-1</sup>
k <sub>s</sub> (non-ionizing organics)	=	cm <sup>3</sup> <sub>water</sub> /g <sub>soil</sub>	THQ	= 1	unitless
k <sub>s</sub> (ionizing organics)	=	cm <sup>3</sup> <sub>water</sub> /g <sub>soil</sub>	TR	=	unitless
k <sub>s</sub> (inorganics)	=	cm <sup>3</sup> <sub>water</sub> /g <sub>soil</sub>	U	=	cm/d
L <sub>s</sub>	= 100	cm	U <sub>air</sub>	= 225	cm/s
LF <sub>sw</sub>	=	(mg/L <sub>water</sub> ) / (mg/kg <sub>soil</sub> )	U <sub>gw</sub>	=	cm/yr
M	= 0.5	mg/cm <sup>2</sup>	VF <sub>p</sub>	=	kg/m <sup>3</sup>
Pe	= 6.9 • 10 <sup>-14</sup>	g/cm <sup>2</sup> -s	VF <sub>samb</sub>	=	(mg/m <sup>3</sup> <sub>air</sub> )/mg/kg <sub>soil</sub> or kg/m <sup>3</sup>
RAF <sub>d</sub>	= 0.5	unitless	VF <sub>ss</sub>	=	kg/m <sup>3</sup>

Symbol		Unit	Symbol		Unit
W	=	cm	$\theta_{as}$	=	$\text{cm}^3_{\text{air}}/\text{cm}^3_{\text{soil}}$
w	=	$\text{g}_{\text{water}}/\text{g}_{\text{soil}}$	$\theta_{ws}$	=	$\text{cm}^3_{\text{water}}/\text{cm}^3_{\text{soil}}$
X	= see below	cm	$\theta_T$	= 0.32	$\text{cm}^3/\text{cm}^3_{\text{soil}}$
$\alpha_x$	=	cm	$\lambda$	= 0.0009	$\text{d}^{-1}$
$\alpha_y$	=	cm	$\pi$	= 3.1416	
$\alpha_z$	=	cm	$\rho_b$	=	$\text{g}/\text{cm}^3$
$\delta_{\text{air}}$	= 200	cm	$\rho_w$	= 1	$\text{g}/\text{cm}^3$
$\delta_{\text{gw}}$	= 200	cm	$\tau$	= $9.46 \cdot 10^8$	s

C<sub>source</sub> Values: (mg/L)

Equation	Result	Unit(s)
R1	=	mg/kg
R2	=	mg/kg
R7	=	mg/kg
R8	=	mg/kg
R12	=	mg/kg
R25	=	mg/L

MW-3 = 0.0574  
 MW-4 = 1.24  
 MW-5 = 0.0735  
 MW-7 = 0.0167  
 MW-8 = 0.0548

**Maximum Predicted Extent of Groundwater Impact (X):**  
 (feet from point source)

MW-3 = 20  
 MW-4 = 51  
 MW-5 = 22  
 MW-7 = 9  
 MW-8 = 19

**RBCA Equation R26**  
**Dissolved Hydrocarbon Concentration Along Centerline**  
**Maximum Predicted Extent of Groundwater Impact Modeling**  
**Groundwater Component of the Groundwater Ingestion Exposure Route**  
1125 Aurora Avenue  
Aurora

**Input Parameters Used in the Solution of Equation R26**

<b>Parameter</b>	<b>Value</b>	<b>Description</b>
First Order Degradation Constant ( $\lambda$ )	Benzene: 0.0009/day Ethylbenzene: 0.003/day	Default Value (Appendix C, Table E)
Aquifer Hydraulic Conductivity (K)	2.131E-05 cm/sec	Site specific value as provided in approved SICR dated September 2, 2021
Hydraulic Gradient (i)	0.03 cm/cm	Site specific value as provided in approved SICR dated February 7, 2022
Total Soil Porosity ( $\theta_T$ )	0.32 cm <sup>3</sup> /cm <sup>3</sup>	Default for sand
Source Width Perpendicular to Groundwater Flow in the Horizontal Plane ( $S_w$ )	6,681.22 cm	Site specific value as provided in approved SICR dated February 7, 2022
Source Width Perpendicular to Groundwater Flow in the Vertical Plane ( $S_d$ )	200 cm	Default Value Appendix C, Table D
Tier 1 Groundwater Remediation Objective for Class I groundwater at the point of human exposure ( $C_x$ )	Benzene: 0.005 mg/L Ethylbenzene: 0.7 mg/L	Appendix B, Table E

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	MW-3
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	02/21/2020
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="58.2"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="19.4"/> cm	
Vertical dispersivity	Az=	<input type="text" value="2.9"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*SQRT(Ay*X))$	B=	<input type="text" value="15.7"/>	
$Sd/(2*SQRT(Az*X))$	C=	<input type="text" value="2.4"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)  Actual erf(C)=

**Solutions**

$C_{(x)}$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	15.71476238	2.428597112
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.162654091	0.556921002
erf(x)=	1	0.999406374

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	MW-4
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	02/21/2020
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )= 1.240 mg/L

Distance along centerline of the plume coming from the source (X)= 50.9 ft = 1,551.43 cm

First order degradation constant ( $\lambda$ )= 0.0009 /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)= 2.131E-05 cm/sec = 1.841 cm/day

Hydraulic gradient (i)= 0.03 m/in

Total soil porosity ( $\theta_r$ )= 0.32 cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )= 219.2 ft = 6,681.22 cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )= 6.56 ft = 200 cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<span style="border: 1px solid black; padding: 2px;">155.1</span> cm	
Transverse dispersivity	Ay=	<span style="border: 1px solid black; padding: 2px;">51.7</span> cm	
Vertical dispersivity	Az=	<span style="border: 1px solid black; padding: 2px;">7.8</span> cm	
Specific discharge	U=	<span style="border: 1px solid black; padding: 2px;">0.2</span> cm/day	
$Sw/(4*\sqrt{A_y*X})$	B=	<span style="border: 1px solid black; padding: 2px;">5.9</span>	
$Sd/(2*\sqrt{A_z*X})$	C=	<span style="border: 1px solid black; padding: 2px;">0.9</span>	
Error function	erf(B)=	<span style="border: 1px solid black; padding: 2px;">1.0</span>	To determine error function values,
Error function	erf(C)=	<span style="border: 1px solid black; padding: 2px;">0.8</span>	see F46 & K46 in the linear interpolation section.

Actual B value= 5.9 Actual C value= 0.9

Automatic calculations : Actual erf(B) 1.0 Actual erf(C)= 0.8

**Solutions**

$C_{(x)}$   
0.005 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	5.896895118	0.911320331
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.341090835	0.770095391
erf(x)=	1	0.802532784

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	MW-5
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	02/21/2020
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion	<b>Analyte:</b> Benzene	
<b>Groundwater Classification:</b>	Class I		

Concentration at the source ( $C_{\text{source}}$ )= 0.074 mg/L

Distance along centerline of the plume coming from the source (X)= 21.4 ft = 652.27 cm

First order degradation constant ( $\lambda$ )= 0.0009 /day if benzene,  $\lambda$ =0.0009/day

Aquifer hydraulic conductivity (K)= 2.131E-05 cm/sec = 1.841 cm/day

Hydraulic gradient (i)= 0.03 m/m

Total soil porosity ( $\theta_r$ )= 0.32 cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )= 219.2 ft = 6,681.22 cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )= 6.56 ft = 200 cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<span style="border: 1px solid black; padding: 2px;">65.2</span> cm	
Transverse dispersivity	Ay=	<span style="border: 1px solid black; padding: 2px;">21.7</span> cm	
Vertical dispersivity	Az=	<span style="border: 1px solid black; padding: 2px;">3.3</span> cm	
Specific discharge	U=	<span style="border: 1px solid black; padding: 2px;">0.2</span> cm/day	
$Sw/(4 \cdot \sqrt{Ay \cdot X})$	B=	<span style="border: 1px solid black; padding: 2px;">14.0</span>	
$Sd/(2 \cdot \sqrt{Az \cdot X})$	C=	<span style="border: 1px solid black; padding: 2px;">2.2</span>	
Error function	erf(B)=	<span style="border: 1px solid black; padding: 2px;">1.0</span>	To determine error function values, see F46 & K46 in the linear interpolation section.
Error function	erf(C)=	<span style="border: 1px solid black; padding: 2px;">1.0</span>	

Actual B value= 14.0 Actual C value= 2.2

Automatic calculations : Actual erf(B) 1.0 Actual erf(C)= 1.0

**Solutions**

$C_{(x)}$   
0.005 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26  
Maximum error in computation =  $1.5 \times 10^{-7}$

x=	14.02579259	2.167579666
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.178739801	0.58476803
erf(x)=	1	0.997826221

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	MW-7
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	12/04/2020
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_r$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="25.9"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="8.6"/> cm	
Vertical dispersivity	Az=	<input type="text" value="1.3"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\sqrt{Ay*X})$	B=	<input type="text" value="35.3"/>	
$Sd/(2*\sqrt{Az*X})$	C=	<input type="text" value="5.5"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)=  Actual erf(C)=

**Solutions**

$C(x)$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26  
Maximum error in computation =  $1.5 \times 10^{-7}$

x=	35.31199547	5.45720057
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.079567817	0.358714753
erf(x)=	1	1

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
<b>Site Name &amp; Location:</b>	1125 Aurora Avenue Aurora	<b>Sample Location:</b>	MW-8
<b>LUST Incident Number(s):</b>	20190483, 20050170	<b>Sample Date:</b>	12/04/2020
<b>Exposure Pathway:</b>	Groundwater Component of Groundwater Ingestion		
<b>Groundwater Classification:</b>	Class I	<b>Analyte:</b>	Benzene

Concentration at the source ( $C_{source}$ )=  mg/L

Distance along centerline of the plume coming from the source (X)=  ft =  cm

First order degradation constant ( $\lambda$ )=  /day if benzene,  $\lambda=0.0009$ /day

Aquifer hydraulic conductivity (K)=  cm/sec =  cm/day

Hydraulic gradient (i)=  m/m

Total soil porosity ( $\theta_T$ )=  cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )=  ft =  cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )=  ft =  cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<input type="text" value="56.8"/> cm	
Transverse dispersivity	Ay=	<input type="text" value="18.9"/> cm	
Vertical dispersivity	Az=	<input type="text" value="2.8"/> cm	
Specific discharge	U=	<input type="text" value="0.2"/> cm/day	
$Sw/(4*\sqrt{A_y*X})$	B=	<input type="text" value="16.1"/>	
$Sd/(2*\sqrt{A_z*X})$	C=	<input type="text" value="2.5"/>	
Error function	erf(B)=	<input type="text" value="1.0"/>	To determine error function values,
Error function	erf(C)=	<input type="text" value="1.0"/>	see F46 & K46 in the linear interpolation section.

Actual B value=  Actual C value=

Automatic calculations : Actual erf(B)=  Actual erf(C)=

**Solutions**

$C(x)$   
 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26  
Maximum error in computation =  $1.5 \times 10^{-7}$

x=	16.09393896	2.48719597
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.159432899	0.551029988
erf(x)=	1	0.999564161

## Illinois Environmental Protection Agency Leaking Underground Storage Tank Program RBCA Input Parameters for Use with Tier 2 Calculations

### A. Site Identification

IEMA Incident # (6- or 8-digit): 20190483, 20050170 IEPA LPC # (10-digit): 0894076105

Site Name: GC Real Estate, LLC.

Site Address (not a P.O. Box): 1125 Aurora Avenue

City: Aurora County: Kane Zip Code: 60505

Leaking UST Technical File

### B. Tier 2 Calculation Information

Equation(s) Used (ex: R12, R14, R26): R26

Contact Information for Individual Who Performed Calculations: Jeff Ogden, Senior Project

Manager, Eagle Environmental Consultants, LLC Phone: (630) 940-2540

Land Use: Not Applicable Soil Type: Sand

Groundwater: ☒ Class I ☐ Class II

Mass Limit: ☐ Yes ☒ No If Yes, then Specify Acreage: ☐ 0.5 ☐ 1 ☐ 2 ☐ 5 ☐ 10 ☐ 30

Result from S18/S28 used in R26? ☐ Yes ☒ No Specify  $C_{\text{source}}$  from S18/S28                      mg/L

- Mass Limit Acreage other than defaults must always be rounded up.
- Failure to use site-specific parameters where allowed could affect payment from the Underground Storage Tank Fund.
- Maps depicting source width, plume dimensions, distance, etc. must also be submitted.
- Inputs must be submitted in the designated unit.

Symbol		Unit	Symbol		Unit	
$AT_c$	=	70	yr	d	=	cm
$AT_\eta$	=		yr	$D^{\text{air}}$	=	cm <sup>2</sup> /s
BW	=	70	kg	$D^{\text{water}}$	=	cm <sup>2</sup> /s
$C_{\text{source}}$	=	see page 3	mg/L	$D_s^{\text{eff}}$	=	cm <sup>2</sup> /s
$C_{(x)}$	=	see page 3	mg/L	ED	=	yr
$C_{(x)}/C_{\text{source}}$	=		unitless	EF	=	d/yr

Symbol		Unit	Symbol		Unit
erf	=	unitless	RAF <sub>d</sub> (PNAs)	= 0.05	unitless
f <sub>oc</sub>	=	g/g	RAF <sub>d</sub> (inorganics)	= 0	unitless
GW <sub>comp</sub>	=	mg/L	RAF <sub>0</sub>	= 1.0	unitless
GW <sub>source</sub>	=	mg/L	RBSL <sub>air</sub> (carcinogenic)	=	µg/m <sup>3</sup>
H'	=	cm <sup>3</sup> <sub>water</sub> /cm <sup>3</sup> <sub>air</sub>	RBSL <sub>air</sub> (noncarcinogenic)	=	µg/m <sup>3</sup>
i	= 0.03	cm/cm	RfD <sub>i</sub>	=	mg/kg-d
I	= 30	cm/yr	RfD <sub>0</sub>	=	mg/kg-d
IR <sub>air</sub>	= 20	m <sup>3</sup> /d	SA	= 3,160	cm <sup>2</sup> /d
IR <sub>soil</sub>	=	mg/d	S <sub>d</sub>	= 200	cm
IR <sub>w</sub>	=	L/d	S <sub>w</sub>	= 6,681.22	cm
K	= 1.841	cm/d for R15, R19, R26; cm/yr for R24	SF <sub>i</sub>	=	(mg/kg-d) <sup>-1</sup>
K <sub>oc</sub>	=	cm <sup>3</sup> /g or L/kg	SF <sub>0</sub>	=	(mg/kg-d) <sup>-1</sup>
k <sub>s</sub> (non-ionizing organics)	=	cm <sup>3</sup> <sub>water</sub> /g <sub>soil</sub>	THQ	= 1	unitless
k <sub>s</sub> (ionizing organics)	=	cm <sup>3</sup> <sub>water</sub> /g <sub>soil</sub>	TR	=	unitless
k <sub>s</sub> (inorganics)	=	cm <sup>3</sup> <sub>water</sub> /g <sub>soil</sub>	U	=	cm/d
L <sub>s</sub>	= 100	cm	U <sub>air</sub>	= 225	cm/s
LF <sub>sw</sub>	=	(mg/L <sub>water</sub> ) / (mg/kg <sub>soil</sub> )	U <sub>gw</sub>	=	cm/yr
M	= 0.5	mg/cm <sup>2</sup>	VF <sub>p</sub>	=	kg/m <sup>3</sup>
Pe	= 6.9 *10 <sup>-14</sup>	g/cm <sup>2</sup> -s	VF <sub>samb</sub>	=	(mg/m <sup>3</sup> <sub>air</sub> )/mg/kg <sub>soil</sub> or kg/m <sup>3</sup>
RAF <sub>d</sub>	= 0.5	unitless	VF <sub>ss</sub>	=	kg/m <sup>3</sup>

Symbol		Unit
W	=	cm
w	=	$g_{\text{water}}/g_{\text{soil}}$
X	= see below	cm
$\alpha_x$	=	cm
$\alpha_y$	=	cm
$\alpha_z$	=	cm
$\delta_{\text{air}}$	= 200	cm
$\delta_{\text{gw}}$	= 200	cm

Symbol		Unit
$\theta_{\text{as}}$	=	$\text{cm}^3_{\text{air}}/\text{cm}^3_{\text{soil}}$
$\theta_{\text{ws}}$	=	$\text{cm}^3_{\text{water}}/\text{cm}^3_{\text{soil}}$
$\theta_T$	= 0.32	$\text{cm}^3/\text{cm}^3_{\text{soil}}$
$\lambda$	= 0.003	$\text{d}^{-1}$
$\pi$	= 3.1416	
$\rho_b$	=	$\text{g}/\text{cm}^3$
$\rho_w$	= 1	$\text{g}/\text{cm}^3$
$\tau$	= $9.46 \cdot 10^8$	s

Equation	Result	Unit(s)
R1	=	mg/kg
R2	=	mg/kg
R7	=	mg/kg
R8	=	mg/kg
R12	=	mg/kg
R25	=	mg/L

C<sub>source</sub> Values: (mg/L)

MW-5 = 1.75

**Maximum Predicted Extent of Groundwater Impact (X):**  
(feet from point source)

MW-5 = 2

**DISSOLVED HYDROCARBON CONCENTRATION ALONG CENTERLINE**  
**MAXIMUM PREDICTED EXTENT OF GROUNDWATER IMPACT MODELING**  
**RBCA EQUATION R26**

Site Details		Sample Details	
Site Name & Location:	1125 Aurora Avenue Aurora	Sample Location:	MW-5
LUST Incident Number(s):	20190483, 20050170	Sample Date:	02/21/2020
Exposure Pathway:	Groundwater Component of Groundwater Ingestion	Analyte: Ethylbenzene	
Groundwater Classification:	Class I		

Concentration at the source ( $C_{source}$ )= 1.750 mg/L

Distance along centerline of the plume coming from the source (X)= 1.9 ft = 57.30 cm

First order degradation constant ( $\lambda$ )= 0.003 /day if ethylbenzene,  $\lambda=0.003/\text{day}$

Aquifer hydraulic conductivity (K)= 2.131E-05 cm/sec = 1.841 cm/day

Hydraulic gradient (i)= 0.03 m/m

Total soil porosity ( $\theta_r$ )= 0.32 cm<sup>3</sup>/cm<sup>3</sup> soil

Source width perpendicular to GW flow direction in horizontal plane ( $S_w$ )= 219.2 ft = 6,681.22 cm

Source width perpendicular to GW flow direction in vertical plane ( $S_d$ )= 6.56 ft = 200 cm (assuming complete mixing)

**Calculated Parameters**

**DO NOT ENTER VALUES HERE!**

Longitudinal dispersivity	Ax=	<span style="border: 1px solid black; padding: 2px;">5.7</span> cm	
Transverse dispersivity	Ay=	<span style="border: 1px solid black; padding: 2px;">1.9</span> cm	
Vertical dispersivity	Az=	<span style="border: 1px solid black; padding: 2px;">0.3</span> cm	
Specific discharge	U=	<span style="border: 1px solid black; padding: 2px;">0.2</span> cm/day	
$S_w/(4*\text{SQRT}(A_y*X))$	B=	<span style="border: 1px solid black; padding: 2px;">159.7</span>	
$S_d/(2*\text{SQRT}(A_z*X))$	C=	<span style="border: 1px solid black; padding: 2px;">24.7</span>	
Error function	erf(B)=	<span style="border: 1px solid black; padding: 2px;">1.0</span>	To determine error function values,
Error function	erf(C)=	<span style="border: 1px solid black; padding: 2px;">1.0</span>	see F46 & K46 in the linear interpolation section.

Actual B value= 159.7 Actual C value= 24.7

Automatic calculations : Actual erf(B) 1.0 Actual erf(C)= 1.0

**Solutions**

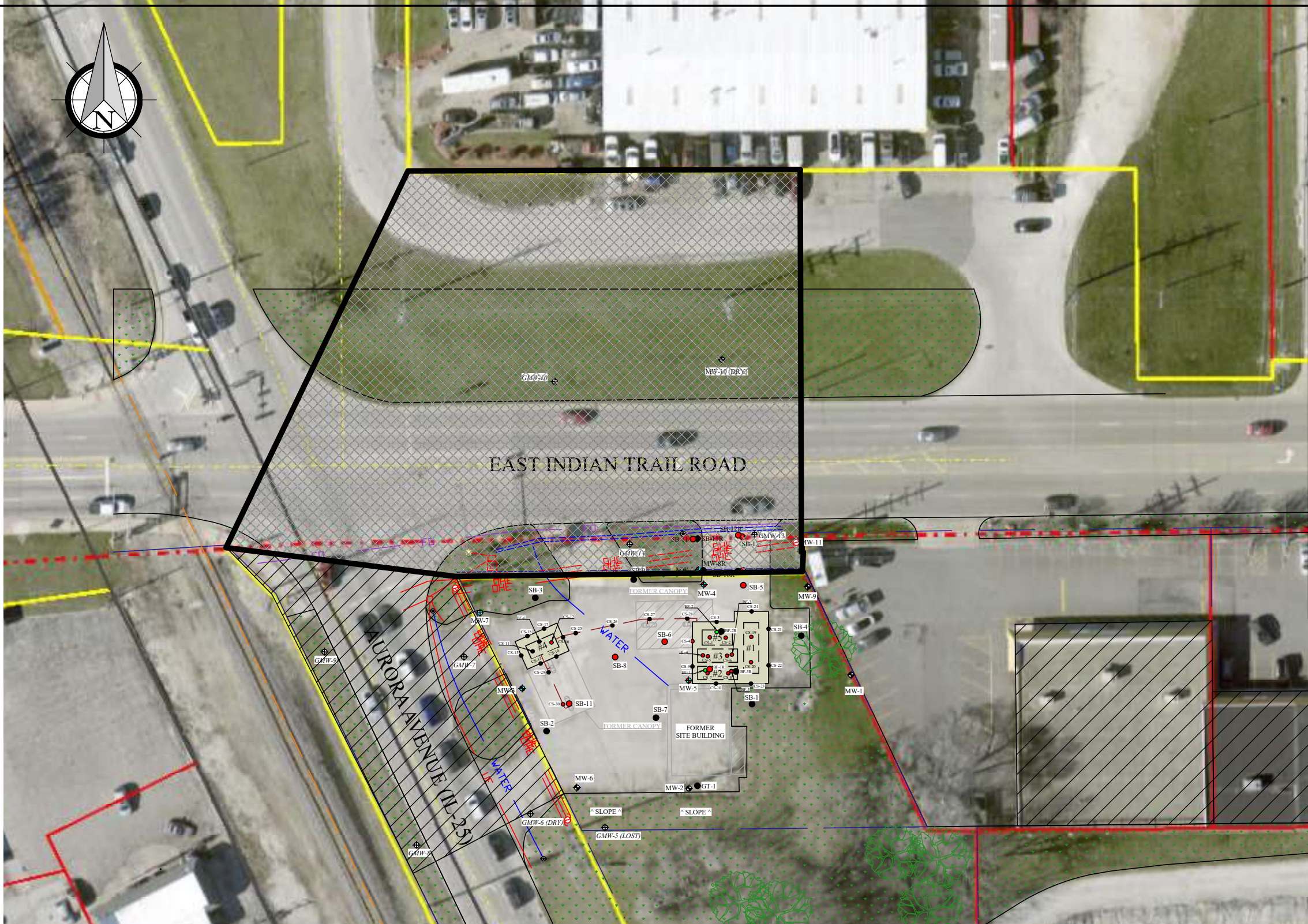
$C_{(x)}$   
0.7 mg/l

Computation of erf(x)

Source: Abramowitz, M. and I. A. Stegun, 1972, Handbook of Mathematical Functions, Dover Publications, New York, page 299, formula 7.1.26

Maximum error in computation =  $1.5 \times 10^{-7}$

x=	159.6552987	24.67351322
p=	0.3275911	0.3275911
a1=	0.254829592	0.254829592
a2=	-0.284496736	-0.284496736
a3=	1.421413741	1.421413741
a4=	-1.453152027	-1.453152027
a5=	1.061405429	1.061405429
t=	0.018761144	0.110097925
erf(x)=	1	1

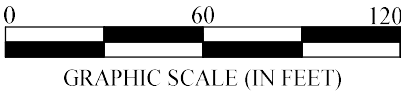


**LEGEND**

- CONFIRMATION SAMPLE LOCATION
  - (●) = ABOVE TIER 1 SRO'S
  - (●) = ABOVE TIER 1 SOIL SATURATION LIMIT
  - (●) = BELOW TIER 1 SRO'S
- SOIL BORING LOCATION
  - (●) = ABOVE TIER 1 SRO'S
  - (●) = BELOW TIER 1 SRO'S
- MONITORING WELL LOCATION
  - (●) = SOIL AND GW BELOW TIER 1 RO'S
  - (●) = SOIL BELOW TIER 1 SRO'S, GW ABOVE TIER 1 GRO'S
  - (●) = SOIL AND GW ABOVE TIER 1 RO'S
  - (●) = GW BELOW TIER 1 RO'S, NO SOIL COLLECTED
  - (●) = GW ABOVE TIER 1 RO'S, NO SOIL COLLECTED
- PROPERTY LINE
- FORMER PRODUCT PIPING RUN
- OHE OVERHEAD ELECTRIC LINE
- UE UNDERGROUND ELECTRIC LINE
- FO UNDERGROUND FIBER OPTIC LINE
- WATER WATER LINE
- RAILROAD LINE
- UTILITY POLE
- LIGHT POLE
- FIRE HYDRANT
- STORM SEWER GRATE

NOTE: MWS LABELED "GMW" WERE INSTALLED BY OTHERS AND CORRESPOND TO LUST INCIDENT #20050170.

- HIGHWAY AUTHORITY AGREEMENT LIMITS (CITY OF AURORA)
- HIGHWAY AUTHORITY AGREEMENT LIMITS (IDOT)



3805 ILLINOIS AVENUE  
ST. CHARLES, ILLINOIS 60174

**PROPOSED HIGHWAY AUTHORITY AGREEMENT LIMITS**

GC REAL ESTATE LLC  
1125 AURORA AVENUE  
AURORA, IL

PREPARED BY: ELMORE	EXHIBIT C	DATE: 02/03/25	PROJECT #: 118109
DRAWN BY: PELLICO	FILE NAME: 118109 - GC AURORA - CAD		